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Torlon® PAI

Design Guide



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Table of Contents

Introduction	5
Torlon® Polyamide-Imide (PAI)	5
Physical Properties	6
Performance Properties	9
Mechanical Properties	9
Tensile and Flexural Strength	9
Effect of ultra-high temperatures	9
Tensile properties per ASTM D638	10
Effect of ultra-low temperatures	10
Flexural Modulus at High Temperature	10
Stress-Strain Relationship	11
Compressive Properties	11
Resistance to Cyclic Stress	12
Fatigue Strength	12
Impact Resistance	13
Fracture Toughness	13
Thermal Stability	14
Thermogravimetric Analysis	14
Effects of Prolonged Thermal Exposure	14
UL Relative Thermal Index	14
Retention of Properties After Thermal Aging	14
Specific Heat	15
Thermal Conductivity	15
Coefficients of Linear Thermal Expansion	15
CLTE test methods	15
Factors affecting CLTE	16
Creep Resistance	16
Flammability	19
Oxygen Index	19
NBS Smoke Density	19
Toxic Gas Emission Test	19
Ignition Properties	19
UL 94 Flammability Standard	20
Horizontal burning test	20
Vertical burn test	20
Flammability	21
Electric Lighting Fixtures	21

Performance in Various Environments	21
Chemical Resistance	21
Resistance to automotive and aviation fluids	23
Chemical Resistance Under Stress	24
Effects of Water	24
Absorption rate	24
Equilibrium absorption at constant humidity	24
Dimensional changes	24
Restoration of dimensions and properties	24
Changes in mechanical and electrical properties	25
Constraints on sudden high temperature exposure	25
Weather-O-meter® Testing	26
Resistance to Gamma Radiation	26
Electrical Properties	27
Torlon® PAI Polymers for Insulating	27
Service in Wear-Resistant Applications	28
An Introduction to Torlon® PAI Wear-Resistant Grades	28
Bearing Design Concepts	28
Wear rate relationship	28
Calculating the pressure and velocity	28
PV limit concept	29
Measuring wear resistance	29
Torlon® PAI Wear-Resistant Grades	30
Effect of Mating Surface on Wear Rate	31
Lubricated Wear Resistance	31
Wear Resistance and Post-Cure	32
Bearing Design	33
Industry and Agency Approvals	34
ASTM D5204 Standard Classification System for Polyamide-imide (PAI) Molding and Extrusion Materials	34
Federal Aviation Administration	34
Military Specification MIL-P-46179A	34
National Aeronautics and Space Administration	34
Society of Automotive Engineers-Aerospace Material Specifications	34
Underwriters Laboratories	34
Vertical flammability	34
Continuous use	34



Structural Design35

Material Efficiency Specific Strength and Modulus35

Geometry and Load Considerations36

Examples of Stress and Deflection Formula

Application 36

Example 1 – Short-term loading 36

Example 2 – Steady load 36

Example 3 – Cyclic load 36

Stress Concentration37

Maximum Working Stresses for Torlon® PAI Resins37

Designing with Torlon® PAI Resin38

Fabrication Options38

Injection Molding 38

Extrusion 38

Compression Molding 38

Post-Curing Torlon® PAI Parts 38

Guidelines for Designing Torlon® PAI Parts 39

Wall section 39

Wall transition 39

Draft angle 39

Cores 39

Ribs 40

Bosses 40

Undercuts 40

Molded-in inserts 40

Threads 40

Holes 40

Secondary Operations41

Joining41

Mechanical Joining Techniques41

Snap-fit: Economical and simple 41

Threaded Fasteners41

Self-tapping screws 41

Molded-in inserts 41

Threaded mechanical inserts 41

Molded-in threads 41

Interference fits 42

Ultrasonic inserts 42

Other mechanical joining techniques 42

Bonding with Adhesives42

Adhesive choice 42

Bonding various Torlon® PAI grades 42

Surface preparation 42

Adhesive application 43

Curing procedure 43

Bond strength of various adhesives 43

Bonding Torlon® PAI parts to metal 43

Guidelines for Machining Parts Made from Torlon® PAI Resin 45

Machined parts should be recured 45

Index 46





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Torlon® Polyamide-Imide (PAI)

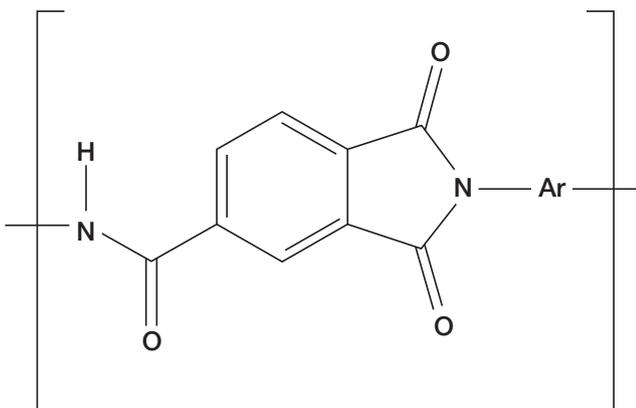
For reliable performance at extremely high temperature and stress, use Torlon® PAI polymers. Parts made of Torlon® PAI polymers perform under conditions generally considered too severe for thermoplastics. That's why parts for the space shuttle, automotive transmissions, and many other critical components have been molded from Torlon® PAI polymers. Torlon® PAI parts meet design challenges across a wide range of industries, including electrical and electronics, business equipment, aerospace, transportation, process, and heavy equipment.

Torlon® PAI polymers has the highest strength and stiffness of any thermoplastic up to 260 °C (500 °F). Unlike many other high-temperature polymers, it offers the added advantage of being injection moldable. That means exact replication and low unit cost, making Torlon® PAI polymers the cost-effective solution to difficult design problems.

This manual introduces the reader to the Torlon® PAI polymer family. Numerous graphs and tables present the physical properties and load-bearing capabilities of Torlon® PAI polymers. A discussion of design guidelines and secondary operations focuses on the practical aspects of fabricating high-performance Torlon® PAI parts. Using this manual, the designer can relate the characteristics of these exceptional resins to his own specific needs.

The general molecular structure of Torlon® PAI is shown in Figure 1.

Figure 1: Structure of polyamide-imide



The variety of applications requiring high-temperature resistance, high strength, and the economies of injection molding has led to the commercialization of several Torlon® PAI grades, each designed to maximize specific properties. These materials can be divided into two categories: high-strength grades and wear-resistant grades. We can also compound Torlon® PAI polymers to meet your specifications. For advice concerning your application, please contact your Solvay representative.

The high-strength grades perform more like metals at elevated temperature, even under considerable stress. These grades are ideally suited for repetitively-used, high-precision mechanical and load-bearing parts.

The inherent lubricity of Torlon® PAI is enhanced with additives in the wear-resistant grades. Moving parts made of Torlon® PAI polymers provide dependable service in lubricated and non-lubricated environments.

Table 1: Torlon® PAI polymers

High Strength	Wear Resistant ⁽¹⁾
4203L ⁽²⁾	4301
5030	4275
7130	4630
	4435
	4645

⁽¹⁾ Products listed in order of increasing wear resistance

⁽²⁾ 4203 has equivalent properties to 4203L

Torlon® PAI polymers off a unique combination of properties:

- Performance from cryogenic to 260 °C (500 °F)
- Outstanding mechanical strength
- Easy fabrication
- Low flammability and smoke generation
- Fatigue strength
- Impact strength
- Creep resistance
- Wear resistance
- Low expansion coefficients
- Excellent thermal stability
- Resistance to aviation and automotive fluids



Physical Properties

High impact strength, exceptional mechanical strength, and excellent retention of these properties in high temperature environments characterize all Torlon® PAI resins.

At room temperature, the tensile and flexural strengths of Torlon® 4203L are about twice that of polycarbonate and polyamide. At 260 °C (500 °F), the tensile and flexural strengths of Torlon® 4203L are almost equal to that of these resins at room temperature. Superior physical properties are retained after long-term exposure to elevated temperature.

These physical properties are typical of injection-molded, post-cured test specimens.



Table 2: Grades and descriptions

Grade	Description
High strength	
4203L ⁽¹⁾	General purpose, unfilled, best impact resistance, most elongation, good mold release, good electrical properties
5030	30 % glass fiber, high stiffness, high strength, good retention of stiffness at high temperatures, very low creep
7130	30 % carbon fiber, best stiffness, best retention of stiffness at high temperatures, best fatigue resistance, electrically conductive
Wear resistant	
4301	General purpose wear-resistance, contains PTFE and graphite
4275	Good wear resistance at high velocities, contains PTFE and graphite
4630	Excellent wear resistance in dry environments, contains PTFE and graphite
4435	Good wear resistance at high velocities and high pressures, contains PTFE and graphite
4645	Excellent wear resistance in lubricated environments, contains PTFE and carbon fiber

⁽¹⁾ 4203 has equivalent properties to 4203L



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Table 3: Typical properties⁽¹⁾ – SI units

Property	Unit	High-Strength Grades			Wear-Resistant Grades					ASTM Test Method
		4203L	5030	7130	4301	4275	4435	4630	4645	
Mechanical										
Tensile strength ⁽²⁾	MPa	152	221	221	113	117	94	81.4	114	D638
Tensile elongation at break	%	7.6	2.3	1.5	3.3	2.6	1.0	1.9	0.8	D638
Tensile modulus	GPa	4.5	14.6	16.5	6.8	8.8	14.5	7.45	18.6	D638
Flexural strength										D790
–196 °C	MPa	282	374	310		200				
23 °C	MPa	244	338	355	219	212	152	131	154	
135 °C	MPa	174	251	263	165	157	129			
232 °C	MPa	120	184	177	113	111	91			
Flexural modulus										D790
–196 °C	GPa	7.9	14.1	24.6		9.6				
23 °C	GPa	5.0	11.7	19.9	6.9	7.3	14.8	6.8	12.4	
135 °C	GPa	3.9	10.7	15.6	5.5	5.6	11.2			
232 °C	GPa	3.6	9.9	13.1	4.5	5.1	10.3			
Compressive strength	MPa	220	260	250	170	120	138	99	157	D695
Compressive modulus	GPa	4.0	7.9	9.9	5.3	4.0	8.5	4.7	5.2	D695
Shear strength	MPa	128	140	120	112	77	60		85	D732
Izod impact strength, 3.2mm	J/m									D256
notched		142	79	47	63	84	43	48	37	
unnotched		1,062	504	340	404	250	219	160	107	
Poisson's ratio		0.45	0.43	0.39	0.39	0.39	0.42			
Thermal										
Heat deflection temperature at 1.82 MPa	°C	278	282	282	279	280	278	279	281	D648
Coefficient of linear thermal expansion	ppm/°C	30.6	16.2	9.0	25.2	25.2	14.4	11.5	14.4	D696
Thermal conductivity	W/mK	0.26	0.37	0.53	0.54	0.65	0.80			C177
Flammability, ⁽³⁾ Underwriters Laboratories		V-0	V-0	V-0	V-0	V-0	V-0			UL 94
Limiting Oxygen Index ⁽³⁾	%	45	51	52	44	45				D2863
Electrical										
Dielectric constant										D150
10 ³ Hz		4.2	4.4		6.0	7.3				
10 ⁶ Hz		3.9	4.2		5.4	6.6				
Dissipation factor										D150
10 ³ Hz		0.026	0.022		0.037	0.059				
10 ⁶ Hz		0.031	0.050		0.042	0.063				
Volume resistivity	ohm·cm	2·10 ¹⁷	2·10 ¹⁷		8·10 ¹⁵	8·10 ¹⁵	2·10 ⁷			D257
Surface resistivity	ohm	5·10 ¹⁸	1·10 ¹⁸		8·10 ¹⁷	4·10 ¹⁷	6·10 ⁶			D257
Dielectric strength, 1 mm	kV/mm	23.6	32.6							D149
General										
Density	g/cm ³	1.42	1.61	1.48	1.46	1.51	1.59	1.56	1.56	D792
Hardness, Rockwell E		86	94	94	72	70	62			D785
Water absorption, 24 hours	%	0.33	0.24	0.26	0.28	0.33	0.12	0.2	0.3	D570

⁽¹⁾ Typical properties – actual properties of individual batches will vary within specification limits.

⁽²⁾ Tensile properties per ASTM D1708 appear in Table 5 on page 10.

⁽³⁾ Methods used to obtain these data measure response to heat and flame under controlled laboratory conditions and may not provide an accurate measure of the hazard under actual fire conditions.



Table 4: Typical properties⁽¹⁾ – US units

Property	Unit	High-Strength Grades			Wear-Resistant Grades				ASTM Test Method	
		4203L	5030	7130	4301	4275	4435	4630		4645
Mechanical										
Tensile strength ⁽²⁾	kpsi	22.0	32.1	32.0	16.4	16.9	13.6	11.8	16.6	D638
Tensile elongation at break	%	7.6	2.3	1.5	3.3	2.6	1.0	1.9	0.8	D638
Tensile modulus	kpsi	650	2,110	2,400	990	1,280	2,100	1,080	2,700	D638
Flexural strength										D790
–321°F	kpsi	41.0	54.4	45.0		29.0				
73 °F	kpsi	34.9	48.3	50.7	31.2	30.2	22.0	19.0	22.4	
275 °F	kpsi	24.8	35.9	37.6	23.5	22.4	18.7			
450 °F	kpsi	17.1	26.2	25.2	16.2	15.8	13.2			
Flexural modulus										D790
–321°F	kpsi	1,140	2,040	3,570		1,390				
73 °F	kpsi	730	1,700	2,400	1,000	1,060	2,150	990	1,800	
275 °F	kpsi	560	1,550	2,270	790	810	1,630			
450 °F	kpsi	520	1,430	1,900	720	740	1,500			
Compressive strength	kpsi	32.1	38.3	36.9	24.1	17.8	20.0	14.4	22.8	D695
Compressive modulus	kpsi	580	1,150	1,430	770	580	1,240	683	760	D695
Shear strength	kpsi	18.5	20.1	17.3	16.1	11.1	8.7		12.4	D732
Izod impact strength, 0.125inch	ft · lbs/in									D256
notched		2.7	1.5	0.9	1.2	1.6	0.8	0.9	0.7	
unnotched		20.0	9.5	6.4	7.6	4.7	4.1	3.0	2.0	
Poisson's ratio		0.45	0.43	0.39	0.39	0.39	0.42			
Thermal										
Heat deflection temperature at 264 psi	°F	532	539	540	534	536	532	535	538	D648
Coefficient of linear thermal expansion	ppm/°F	17	9	5	14	14	8	20	8	D696
Thermal conductivity	Btu · in/ hr · ft ² · °F	1.8	2.5	3.6	3.7	4.5	5.6			C177
Flammability, ⁽³⁾ Underwriters Laboratories		V-0	V-0	V-0	V-0	V-0	V-0			UL 94
Limiting Oxygen Index ⁽³⁾	%	45	51	52	44	45				D2863
Electrical										
Dielectric constant										D150
10 ³ Hz		4.2	4.4		6.0	7.3				
10 ⁶ Hz		3.9	4.2		5.4	6.6				
Dissipation factor										D150
10 ³ Hz		0.026	0.022		0.037	0.059				
10 ⁶ Hz		0.031	0.050		0.042	0.063				
Volume resistivity	ohm · cm	2 · 10 ¹⁷	2 · 10 ¹⁷		8 · 10 ¹⁵	8 · 10 ¹⁵	2 · 10 ⁷			D257
Surface resistivity	ohm	5 · 10 ¹⁸	1 · 10 ¹⁸		8 · 10 ¹⁷	4 · 10 ¹⁷	6 · 10 ⁶			D257
Dielectric strength, 0.040 in	V/mil	580	840							D149
General										
Density	lb/in ³	0.051	0.058	0.054	0.053	0.054	0.057	0.056	0.056	D792
Hardness, Rockwell E		86	94	94	72	70	62			D785
Water absorption, 24 hours	%	0.33	0.24	0.26	0.28	0.33	0.12	0.2	0.3	D570

⁽¹⁾ Typical properties – actual properties of individual batches will vary within specification limits.

⁽²⁾ Tensile properties per ASTM D1708 appear in Table 5 on page 10.

⁽³⁾ Methods used to obtain these data measure response to heat and flame under controlled laboratory conditions and do not provide an accurate measure of the hazard under actual fire conditions.



Performance Properties

The unrivaled properties of Torlon® PAI polymers meet the requirements of the most demanding applications. Strength retention over a wide range of temperatures and sustained stress, low creep, flame resistance, outstanding electrical properties, and exceptional integrity in severe environments place Torlon® PAI in the category of ultra-high performance polymers.

Mechanical Properties

Tensile and Flexural Strength

Effect of ultra-high temperatures

Torlon® PAI can be used in applications previously considered too demanding for many other plastics because of its outstanding tensile and flexural strength and its ability to retain these properties in continuous service at temperatures in excess of 232 °C (450 °F).

While many competitive resins can claim “excursions” up to 260 °C (500 °F), Torlon® PAI polymers function with integrity at extremely high temperatures, as shown in Figures 2 and 3.

Even at 204 °C (400 °F), both tensile and flexural strength of Torlon® PAI polymers are better than other high performance resins. Figures 4 and 5 compare reinforced Torlon® PAI polymers to other high performance reinforced resins.

Figure 2: Tensile strength of Torlon® PAI over a broad temperature range

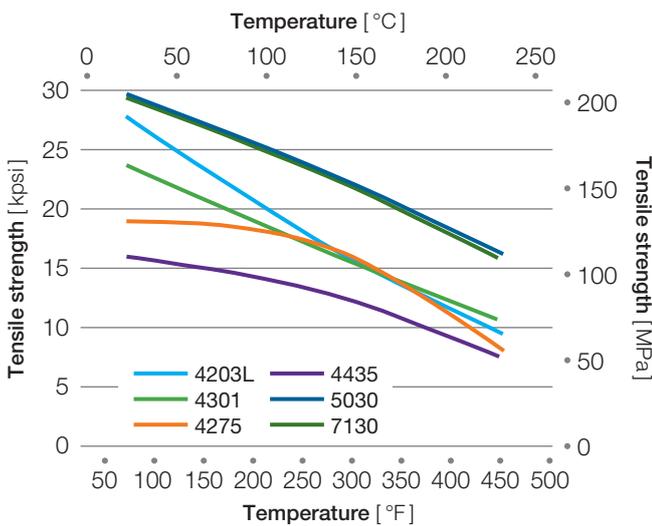


Figure 3: Flexural strength of Torlon® PAI over a broad temperature range

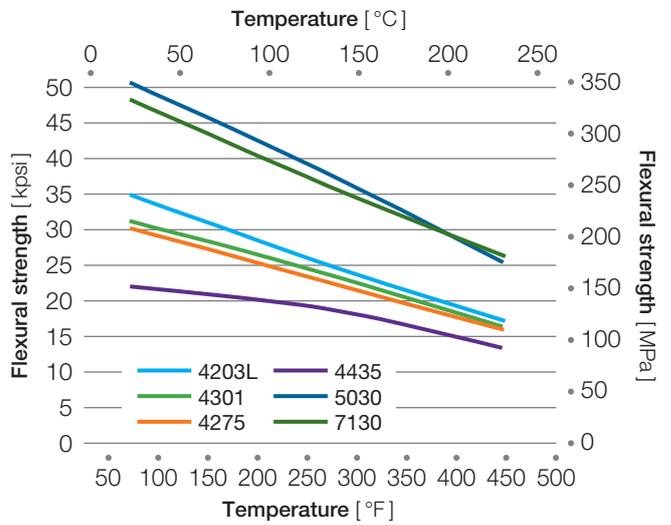


Figure 4: Tensile strength of reinforced Torlon® PAI surpasses competitive reinforced polymers at 204 °C (400 °F)

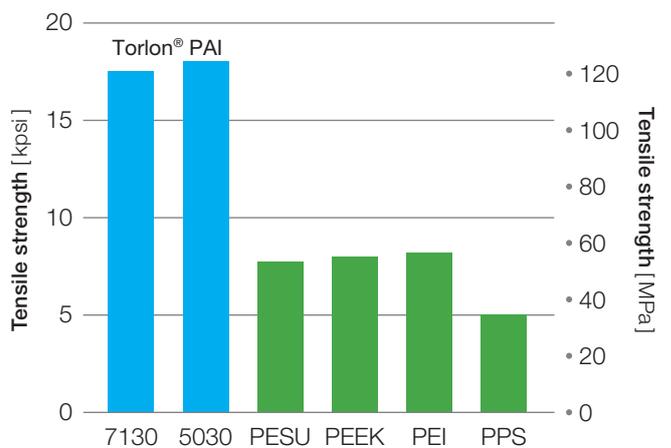
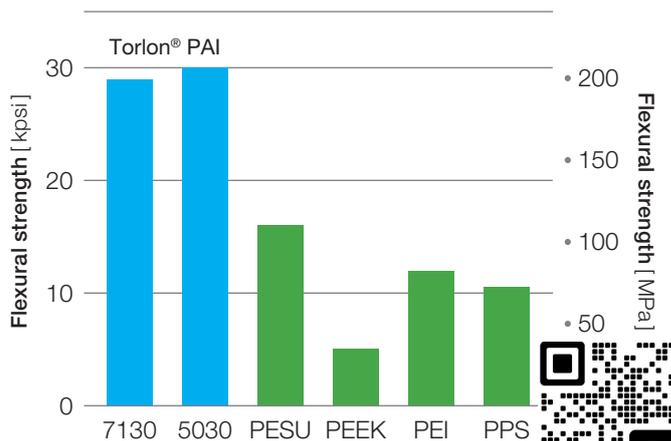


Figure 5: Flexural strength of reinforced Torlon® PAI resins surpasses competitive reinforced resins at 204 °C (400 °F)



Tensile properties per ASTM D638

Tensile properties reported in the preceding section were obtained in accordance with ASTM D638. Since tensile properties are frequently measured using ASTM D1708, Torlon® PAI polymers were also tested in accordance with this method. The data appears in Table 5.

Effect of ultra-low temperatures

At the other end of the temperature spectrum, Torlon® PAI polymers do not become brittle as do other resins. Table 6 shows Torlon® PAI resins have excellent properties under cryogenic conditions.

Table 5: Tensile properties per ASTM D1708

Property	Unit	Grade					
		4203L	4301	4275	4435	5030	7130
Tensile strength							
23 °C	MPa	192	164	131	110	205	203
73 °F	kpsi	27.8	23.7	19.0	16.0	29.7	29.4
135 °C	MPa	117	113	116	90	160	158
275 °F	kpsi	16.9	16.3	16.9	13.0	23.1	22.8
232 °C	MPa	66	73	56	52	113	108
450 °F	kpsi	9.5	10.6	8.1	7.5	16.3	15.7
Tensile elongation at break							
23 °C	%	15	7	7	6	7	6
73 °F	%						
135 °C	%	21	20	15	4	15	14
275 °F	%						
232 °C	%	22	17	17	3	12	11
450 °F	%						
Tensile modulus							
23 °C	GPa	4.5	6.8	8.8	14.5	14.6	16.5
73 °F	kpsi	700	950	1,130	1,410	1,560	2,400

Flexural Modulus at High Temperature

Torlon® PAI has high modulus, making it a good replacement for metal where stiffness is crucial to performance. Torlon® PAI parts can provide equivalent stiffness at significantly lower weight. Excellent retention of part stiffness and resistance to creep or cold flow is predicted from the high and essentially constant modulus of Torlon® PAI resins, even at 232 °C (450 °F), as shown in Figure 6. Unlike competitive materials, which lose stiffness at higher temperatures, Torlon® PAI polymers have a high modulus at elevated temperatures, as Figure 7 demonstrates.

Table 6: Properties of Torlon® PAI molding resins at -196 °C (-321 °F)

Property	Unit	Grade			
		4203L	4275	5030	7130
Tensile strength ⁽¹⁾	MPa	216	129	203	157
	kpsi	31.5	18.8	29.5	22.8
Elongation at break ⁽¹⁾	%	6	3	4	3
Flexural strength ⁽²⁾	MPa	282	200	374	310
	kpsi	41.0	29.0	54.4	45.0
Flexural modulus ⁽²⁾	GPa	7.8	9.6	14.0	24.6
	kpsi	1,140	1,390	2,040	3,570

⁽¹⁾ ASTM D1708

⁽²⁾ ASTM D790

Figure 6: Flexural modulus of Torlon® PAI polymers over a broad temperature range

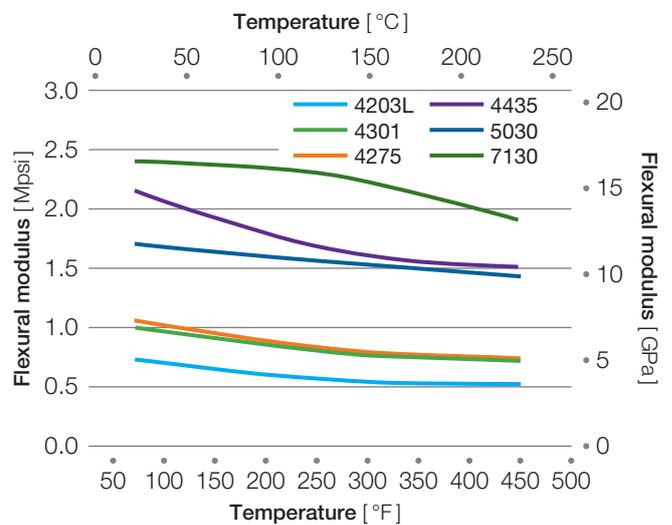
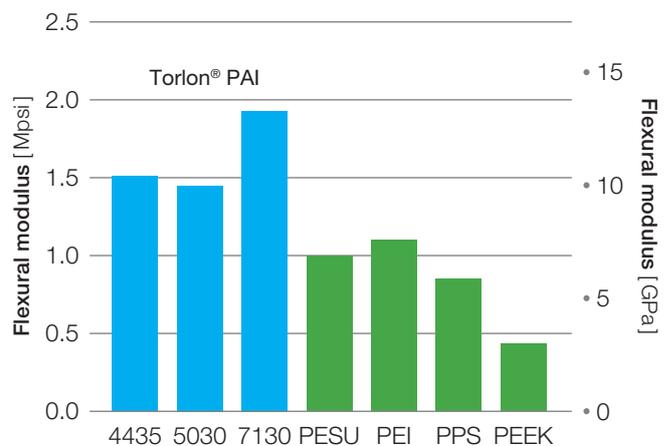


Figure 7: Flexural modulus of reinforced Torlon® PAI is superior to competitive reinforced resins at 204 °C (400 °F)



Stress-Strain Relationship

Torlon® PAI does not yield at room temperature, therefore, strain at failure or rupture is recorded as the elongation. Figure 8 shows the stress-strain relationship for Torlon® PAI grades at room temperature. Figure 9 shows just the first 1% strain – the nearly linear (“Hookean”) portion of the room temperature curve. Figure 10 shows the initial portion of stress-strain curve measured at 200 °C (392 °F).

Figure 8: Stress-strain in tension for Torlon® PAI at 23 °C (73 °F) tested on ASTM D638 Type 1 specimens

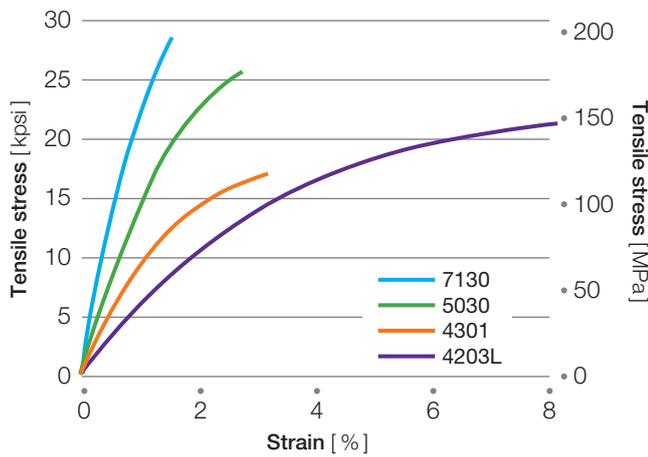


Figure 9: Stress-strain detail of Figure 8 at 23 °C (73 °F)

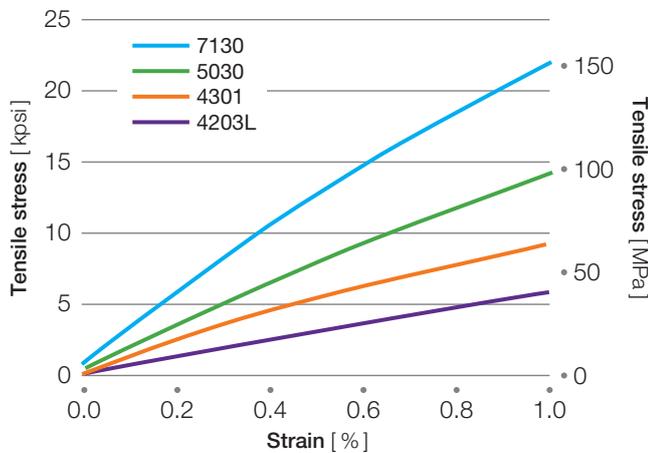


Figure 10: Stress-strain in tension for various Torlon® PAI resins at 200 °C (392 °F)

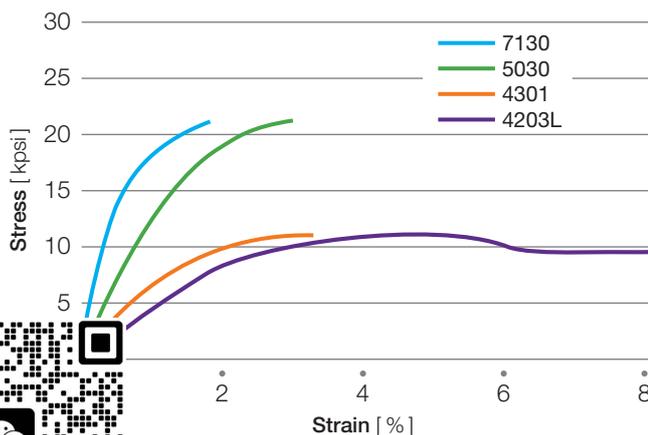
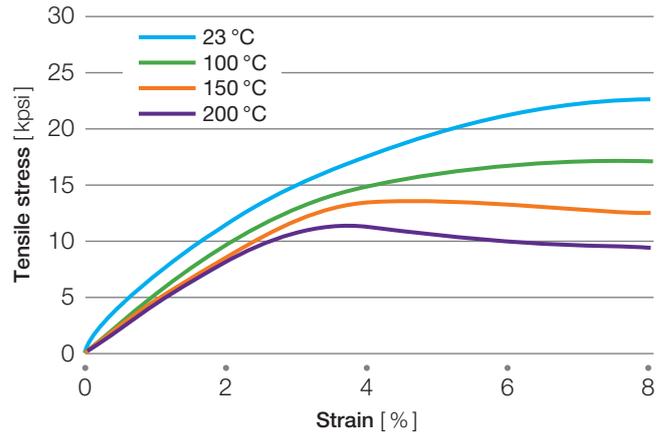


Figure 11: Stress-strain in tension for Torlon® 4203LF over a broad temperature range



Compressive Properties

In addition to offering retention of tensile strength at high temperatures, Torlon® PAI also offers retention of compressive strength at high temperatures. The compressive strength of unreinforced Torlon® PAI rivals that of glass fiber and carbon fiber reinforced high-performance polymers. Torlon® PAI is able to offer elastic compression without the yield or creep that can cause compression set because of its outstanding elastic recovery. For applications requiring higher strength and wear resistance, glass and carbon fiber reinforced grades as well as wear-resistant grades are available.

The compressive properties of Torlon® PAI combined with excellent creep and fatigue resistance make it a superior sealing material in applications such as seal rings, hydraulic poppets, brake tappets, check balls, thrust washers, and compressor plates.

Table 7: Compressive properties (ASTM D695)

Property	Unit	Grade					
		4203L	4601	4630	4645	5030	7130
Compressive strength							
23 °C	MPa	172	165	96	124	214	234
73 °F	kpsi	25	24	14	18	31	34
100 °C	MPa	131	124	83	124	165	186
212 °F	kpsi	19	18	12	18	24	27
150 °C	MPa	103	103	76	110	138	158
302 °F	kpsi	15	15	11	16	20	23
200 °C	MPa	83	83	62	90	110	124
392 °F	kpsi	12	12	9	13	16	18
Compressive modulus							
23 °C	MPa	3,163	3,114	4,706	5,236	4,892	6,139
73 °F	kpsi	459	452	683	760	710	891
100 °C	MPa	2,191	2,122	2,026	3,645	3,273	3,803
212 °F	kpsi	318	308	294	529	475	552
150 °C	MPa	2,136	2,067	2,115	3,149	3,087	3,790
302 °F	kpsi	310	300	307	457	448	550
200 °C	MPa	2,067	2,046	2,019	3,383		
392 °F	kpsi	300	297	293	491		



Resistance to Cyclic Stress

Fatigue Strength

When a material is stressed cyclically, failure will occur at stress levels lower than the material's ultimate strength. Resistance to failure under cyclical loading or vibration, called fatigue strength, is an important design consideration. Torlon® PAI polymers offer excellent fatigue strength in both the tensile mode and the very severe flexural mode, a form of reverse bending.

S-N diagrams, showing maximum stress versus cycles to failure, are useful in predicting product life. The maximum stress using the anticipated force, appropriate stress concentration factors, and section modulus is determined. The maximum stress is then compared to the fatigue strength S-N curve for the applicable environment to determine the maximum cyclic stress the material can be expected to withstand.

The values obtained in fatigue testing are influenced by the specimen and test method; therefore, the values should serve as guidelines, not absolute values. Torlon® PAI parts resist cyclic stress. Torlon® 7130, a carbon fiber reinforced grade, has exceptional fatigue strength, and it is superior to competitive engineering resins. The S-N curves for selected Torlon® PAI grades in Figure 12 show that even after 10,000,000 cycles, Torlon® PAI has excellent resistance to cyclical stress in the flexural mode. Figure 13 demonstrates the integrity of Torlon® 7130 under tension/tension cyclical stress. At lower frequencies, the fatigue strength of Torlon® 7130 is even higher, as shown in Figure 14.

Even at high temperature, Torlon® PAI polymers maintain strength under cyclic stress. Flexural fatigue tests were run at 177 °C (350 °F) on specimens preconditioned at that temperature. The results, shown in Figure 15, suggest that Torlon® PAI polymers are suitable for applications requiring fatigue resistance at high temperature.

Figure 12: Flexural fatigue strength of Torlon® PAI resins at 30 Hz

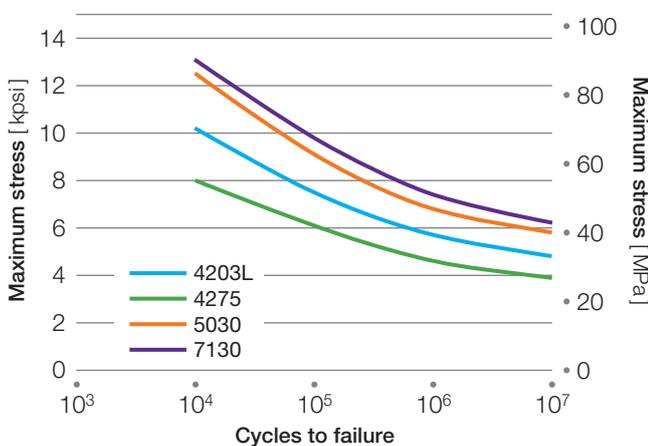


Figure 13: Tension/tension fatigue strength of Torlon® 7130 and 4230L at 30 Hz, A ratio: 0.90

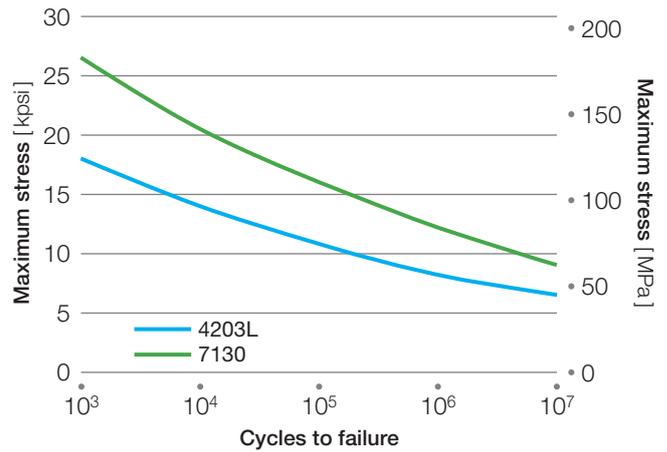


Figure 14: Tension/tension low cycle fatigue strength of Torlon® 7130 at 2 Hz, A ratio: 0.90

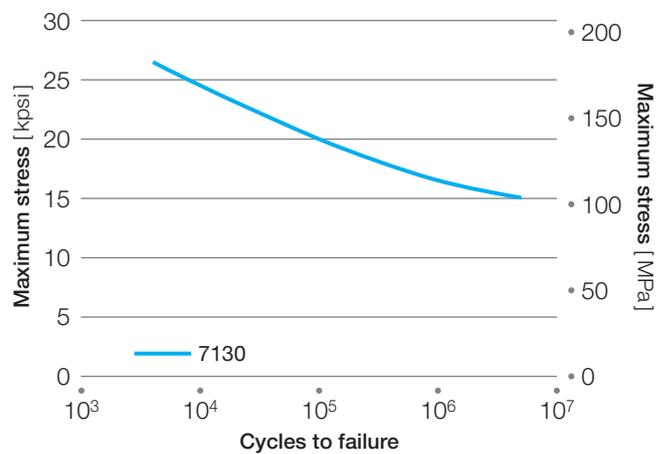
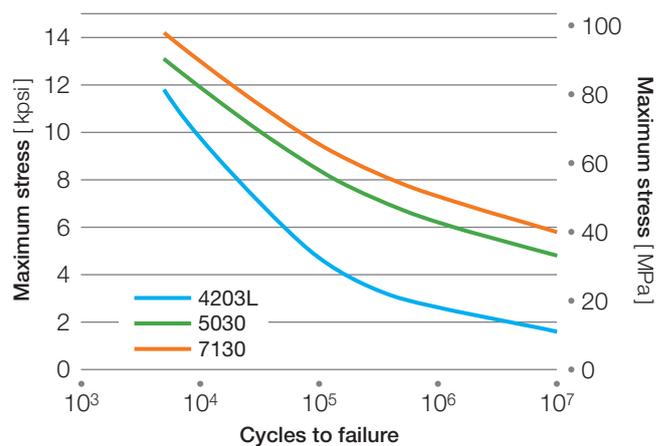


Figure 15: High-temperature flexural fatigue strength of Torlon® PAI resins at 177 °C (350 °F), 30 Hz



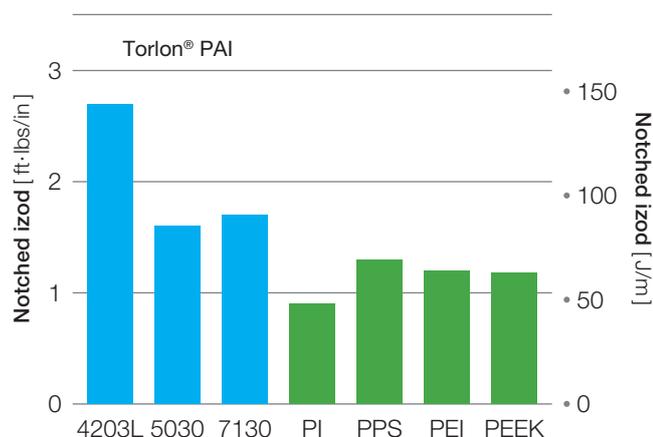
Design Guide



Table 8: Izod impact resistance of 3.2 mm (0.125 inch) bars of Torlon® PAI resins

Grade	Notched		Unnotched	
	J/m	ft·lb/inch	J/m	ft·lb/inch
4203L	142	2.7	1,062	20.0
4301	63	1.2	404	7.6
4275	84	1.6	250	4.7
4435	42	0.8	220	4.1
5030	79	1.5	504	9.5
7130	47	0.9	340	6.4

Figure 16: Izod impact resistance of Torlon® PAI resins vs. competitive materials



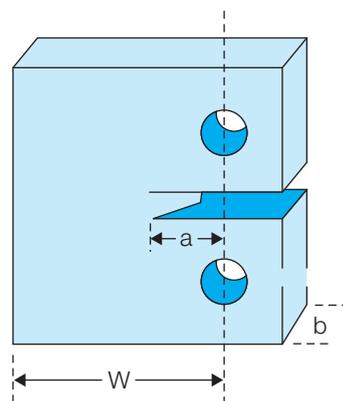
Impact Resistance

Torlon® PAI resins absorb impact energy better than most high-modulus plastics. In tests using the notched Izod method (ASTM D256), Torlon® PAI resins outperformed other high-temperature resins (Figure 16). Table 8 summarizes both notched and unnotched impact data for Torlon® PAI resins.

Fracture Toughness

Fracture toughness can be assessed by measuring the fracture energy (G_{Ic}) of a polymer. The Naval Research Laboratory (NRL) uses a compact tension specimen (Figure 17) to determine G_{Ic} which measures a polymer's ability to absorb and dissipate impact energy without fracturing; larger values correspond to higher fracture toughness. Table 9 shows selected data from NRL Memorandum Report 5231 (February 22, 1984). As expected, thermoset polymers cannot absorb and dissipate impact energy as well as thermoplastics and consequently have lower fracture energies. Torlon® PAI exhibits outstanding fracture toughness, with a G_{Ic} of 3.4 kJ/m^2 (1.6 $\text{ft}\cdot\text{lb/in}^2$). Glass transition temperatures (T_g) are included in the table to indicate the trade off between fracture toughness and useful temperature range. Torlon®

Figure 17: Compact tension specimen



$$G_{Ic} = \frac{Y^2 P_c^2 a}{EW^2 b^2}$$

Where:

$$Y = 29.6 - 186(a/w) + 656(a/w)^2 - 1017(a/w)^3 + 639(a/w)^4$$

P = Critical fracture load

a = Crack length

E = Sample modulus

Table 9: Torlon® PAI balances fracture toughness and high glass transition temperature

Polymer	Fracture Energy		T_g	
	[kJ/m ²]	[ft·lb/in ²]	[°C]	[°F]
Thermosets				
Polyimide-1	0.20	0.095	350	662
Polyimide-2	0.12	0.057	360	680
Tetrafunctional epoxy	0.076	0.036	260	500
Thermoplastics				
Polyamide-imide	3.4	1.6	275	527
Polysulfone	3.1	1.5	174	345
Polyethersulfone	2.6	1.2	230	446
Polyimide-3	0.81	0.38	326	619
Polyimide-4	2.1	1.0	365	689
Polyphenylene sulfide	0.21	0.10	—	—

acterized by a balance of toughness and high T_g .

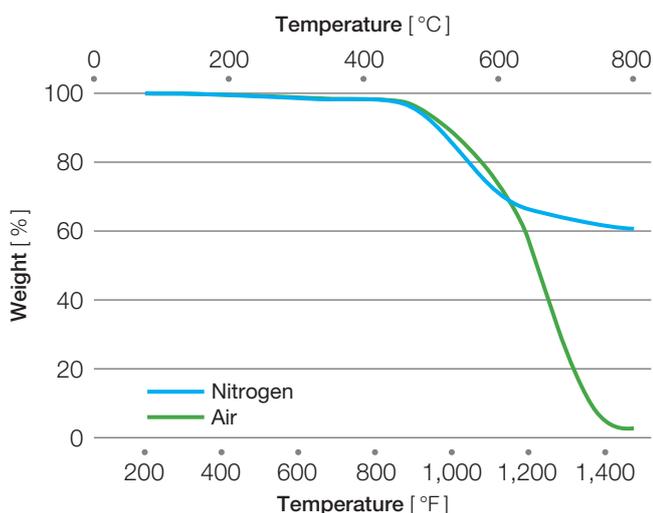


Thermal Stability

Thermogravimetric Analysis

Torlon® PAI resins are exceptionally stable over a wide range of temperatures. When heated at a rate of 10 °C (18 °F) per minute in air or nitrogen atmospheres, Torlon® 4203L shows virtually no weight loss over its normal service temperatures and well beyond, as shown in Figure 18.

Figure 18: Thermogravimetric analysis of Torlon® 4203L



Effects of Prolonged Thermal Exposure

UL Relative Thermal Index

The UL Relative Thermal Index provides an estimate of the maximum continuous-use temperature and is defined by the method prescribed by Underwriters Laboratories.

Initial properties, including tensile strength, impact strength, dielectric strength, arc resistance, dimensional stability, and flammability, are determined for the test material. For each property and each aging temperature, a record is kept of the elapsed time and the change in that property as a percent of initial. The “end-of-life” for a property is the time required at the aging temperature to reach 50% of initial. End-of-life points are plotted and regression applied to predict “life expectancy” at any operating temperature. The Relative Thermal Index is that temperature at which life expectancy is 100,000 hours. Torlon® PAI polymers were tested in accordance with the above procedure for 50% degradation of dielectric strength (Electrical), Izod impact (mechanical with impact), and tensile strength (mechanical without impact). The other properties did not change significantly.

Table 10: Relative thermal indices of Torlon® PAI resins

Grade	Minimum Thickness		Mechanical					
			Electrical		With Impact		Without Impact	
	[mm]	[inch]	[°C]	[°F]	[°C]	[°F]	[°C]	[°F]
4203L	0.81	0.031	220	428			210	410
	1.2	0.047	220	428			210	410
	2.4	0.096	220	428			210	410
	3.0	0.118	220	428	200	392	220	428
4301	3.0	0.118			200	392	200	392
5030	1.5	0.062	220	428				
	2.4	0.096	220	428				
	3.0	0.118	220	428	200	392	220	428

The UL Relative Thermal Index predicts at least 100,000 hours of useful life at the index temperature. Torlon® PAI polymers have UL relative thermal indices as high as 220 °C (428 °F), which is equivalent to more than 11 years of continuous use at 220 °C (428 °F). This is significantly higher than most high-temperature engineering resins. Table 10 summarizes the relative thermal indices of Torlon® PAI grades 4203L, 4301, and 5030. Refer to Underwriters Laboratories web site for the latest information.

Retention of Properties After Thermal Aging

Torlon® PAI resists chemical breakdown and retains high strength after prolonged thermal exposure. One method for determining the thermal stability of polymers is to measure mechanical properties of samples after aging at elevated temperatures.

Injection molded and post-cured ASTM D1708 tensile bars with 3.125-mm (0.125-inch) thicknesses were aged in forced air ovens at 250 °C (482 °F). Specimens were periodically removed from the ovens, conditioned at 23 °C (73 °F) and 50% relative humidity, and then tested for tensile strength.

Torlon® PAI resins retain strength after long-term aging at high temperature, as shown in Figure 19. After 10,000 hours, tensile strengths of Torlon® PAI polymers exceed the ultimate strength of many competitive resins. Torlon® 4203L, for example, still has tensile strength of over 170 MPa (25,000 psi). It is interesting to note that initially the specimens actually increase in tensile strength, because even greater strength is attained beyond the standard post cure.



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Figure 19: Torlon® PAI resins retain strength after thermal aging at 250 °C (482 °F)

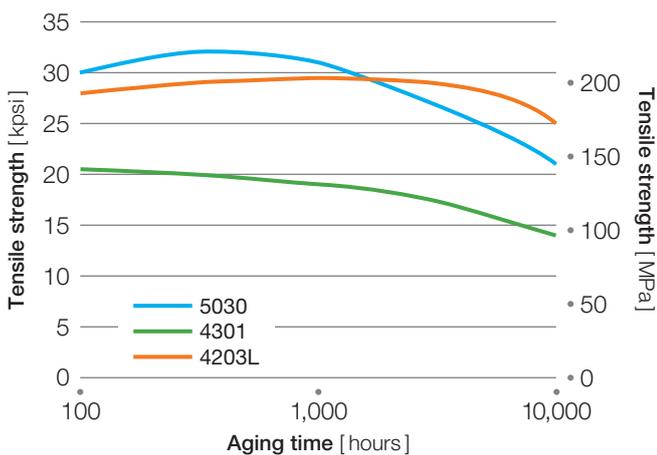


Table 11: Torlon® 4203L retention of properties after thermal aging at 250 °C (482 °F)

Property	Unit	Hours		
		2,000	12,000	17,000
Dielectric strength ⁽¹⁾	kV/mm			25.7
Flammability ⁽²⁾	UL 94	V-0	V-0	V-0
Dimensional change ⁽²⁾	%	0.0	0.5	0.9
Tensile strength retained ⁽²⁾	%	110	86	67
Izod impact strength retained ⁽²⁾	%	101	67	38

⁽¹⁾ Specimen thickness 0.9 mm (0.035 inches)

⁽²⁾ Specimen thickness 3.2 mm (0.125 inches)

Torlon® PAI polymers maintain exceptional electrical and mechanical properties and UL flammability ratings after long-term heat aging. Table 11 demonstrates that Torlon® 4203L is still suitable for demanding applications even after extended exposure to 250 °C (482 °F).

Specific Heat

Specific heat as a function of temperature was determined using a differential scanning calorimeter. The data for four Torlon® PAI grades at four temperatures are presented in Table 12.

Thermal Conductivity

Torlon® PAI resins have low thermal conductivity, making them suitable for applications requiring thermal isolation. Torlon® PAI heat shields protect critical sealing elements from high temperatures, and they protect sensitive instrument elements from heat loss. Table 13 shows the thermal conductivity of Torlon® PAI resins measured using ASTM C177 with 1.6 mm (0.06 inches) thick specimens and a cold plate temperature of 50 °C (122 °F) and a hot plate temperature of 100 °C (212 °F).

Table 12: Specific heat of Torlon® PAI resins

Temperature [°C (°F)]	Specific Heat [cal/gm°C]			
	4203L	4301	5030	7130
25 (77)	0.242	0.240	0.229	0.230
100 (212)	0.298	0.298	0.276	0.285
200 (392)	0.362	0.359	0.327	0.346
250 (482)	0.394	0.385	0.353	0.375

Table 13: Thermal conductivity of Torlon® PAI resins

Grade	Thermal Conductivity	
	[Btu·inch/hr·ft ² ·°F]	[W/m·K]
4203L	1.8	0.26
4301	3.7	0.54
4275	4.5	0.65
4435	5.6	0.80
5030	2.5	0.37
7130	3.6	0.53

Coefficients of Linear Thermal Expansion

The Coefficient of Linear Thermal Expansion (CLTE) measures the rate of expansion of a solid mass as its temperature increases. The higher the material's CLTE, the more it will expand and contract upon changes in temperature.

CLTE can influence the ability to achieve tight tolerances for mating parts or surfaces. It can also affect adhesion to coated or over-molded substrates and relate to stress in parts or coatings used over a broad temperature range.

CLTE test methods

There are several test methods used for measuring CLTE. ASTM D696 (–30 °C to 30 °C) and ASTM E228 (–180 °C to 900 °C) follow a dilatometric method in which a vitreous silica rod and tube slide within each other, attached to a measurement device. Test Method ASTM E831 (–120 °C to 900 °C) and ISO 11359-2 offer a thermal-mechanical analysis in which a linear motion sensor is used together with a probe to measure displacement.



Factors affecting CLTE

It is important to realize that CLTE can vary depending on sample size and preparation. Therefore, a thorough evaluation of CLTE data involves consideration of several factors.

Part thickness

Thermal expansion is not linear with thickness. Heat flow and temperature differential across thick parts can inflate or deflate CLTE.

Temperature range and phase changes

The phase of a polymer can change across its glass transition temperature (T_g). Above the T_g , molecular mobility increases and expansion rate increases.

Processing parameters

Factors such as mold temperature and annealing can affect crystallinity and stresses in parts, which can affect CLTE. It is important to cure Torlon® PAI resin properly to minimize CLTE.

Reinforcements

High aspect ratio fillers such as glass and carbon fibers can lead to anisotropic CLTE. Orientation of fillers can be affected by processing parameters and mold design.

Table 14: CLTE for Torlon® PAI resins and selected metals⁽¹⁾

	CLTE	
	[ppm/°C]	[ppm/°F]
Torlon® 7130	9.0	5.0
Inconel X, annealed	12.1	6.7
Plain carbon steel AISI-SAE 1020	12.1	6.7
Titanium 6-2-4-2	12.6	7.0
Torlon® 5030	16.2	9.0
Copper	16.7	9.3
Stainless steel, type 304	17.3	9.6
Commercial bronze, 90%, C2200	18.4	10.2
Aluminum alloy 2017, annealed, ASTM B221	22.9	12.7
Torlon® 4275	25.2	14.0
Torlon® 4301	25.2	14.0
Aluminum alloy 7075	26.0	14.4
Torlon® 4203L	30.6	17.0

⁽¹⁾ The CLTE data for Torlon® PAI resins were determined per ASTM D696, over a temperature range of 24 °C to 149 °C (75 °F to 300 °F). CLTE data for metals are from the CRC Handbook of Chemistry and Physics, 54th ed. and Materials Engineering, 1984 Materials Selector edition, Dec. 1983.

Part geometry

Specimens of different thickness can yield different results depending on thermal conductivity. The most useful CLTE measurements will be made on parts of similar thickness to application dimensions, prepared in a similar way.

In general, parts should be designed such that they will be properly sized at end-use temperature. Molds should be designed accordingly, with clearances and tolerances taking expansion at temperature into account.

Note that while CLTE data is reported in the direction of flow, or transverse to the direction of the flow, actual applications will typically need to factor in the effect of CLTE in all directions.

Due to its amorphous nature, Torlon® PAI offers a highly isotropic CLTE with very high consistency over a broad temperature range. As shown in Table 14, the thermal expansion of filled Torlon® PAI resin nearly matches that of common metals.

Creep Resistance

When a material is subjected to a stress, it will deform or exhibit strain. The immediate strain can be calculated from the appropriate modulus. If the stress is continually applied for an extended time, additional strain will result which is known as creep strain. Torlon® PAI resists creep and handles stress more like a metal than a plastic. To get measurable creep, Torlon® PAI must be stressed beyond the ultimate strength of most other plastics. The designer must consider the long-term creep behavior of plastics under the expected stress and temperature conditions of the proposed application. Figures 20 through 24 summarize selected data from tensile creep tests (ASTM D2990) at applied stresses of 34.5 MPa, 68.9 MPa, and 103.4 MPa (5 kpsi, 10 kpsi and 15 kpsi) at room temperature.

Figures 25 through 29 show this data for tests performed at 204 °C (400 °F). Non-reinforced Torlon® PAI grades may creep or rupture at extremely high temperatures – over 204 °C (400 °F) – when stress exceeds 34.5 MPa (5 kpsi). For these applications, a reinforced grade is recommended.



Figure 20: Torlon® 4203L strain vs. time at 23°C (73°F)

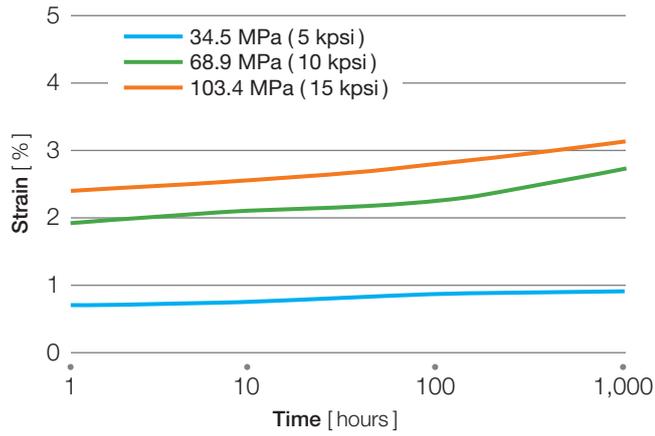


Figure 21: Torlon® 4275 strain vs. time at 23°C (73°F)

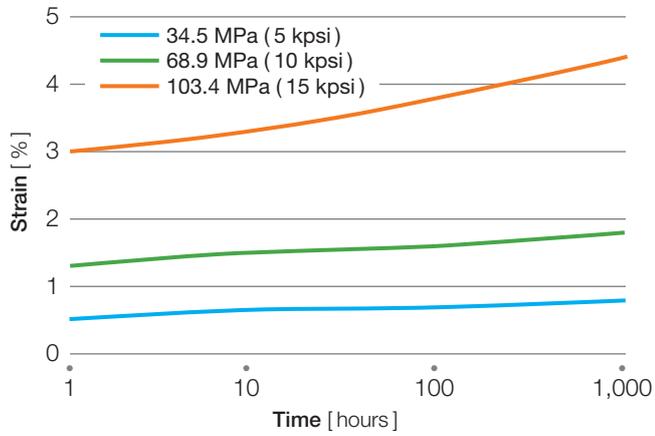


Figure 22: Torlon® 4301 strain vs. time at 23°C (73°F)

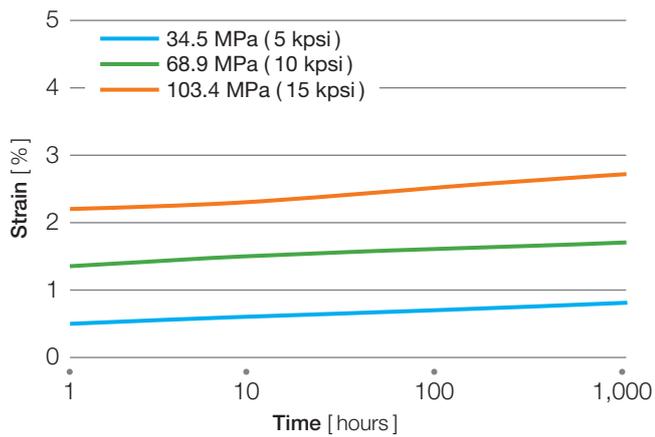


Figure 23: Torlon® 5030 strain vs. time at 23°C (73°F)

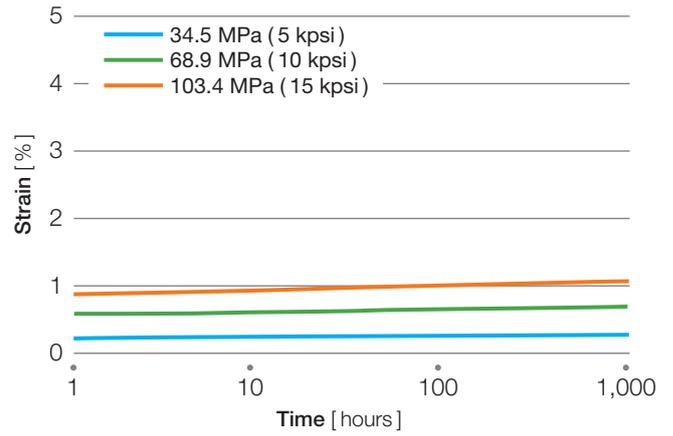


Figure 24: Torlon® 7130 strain vs. time at 23°C (73°F)

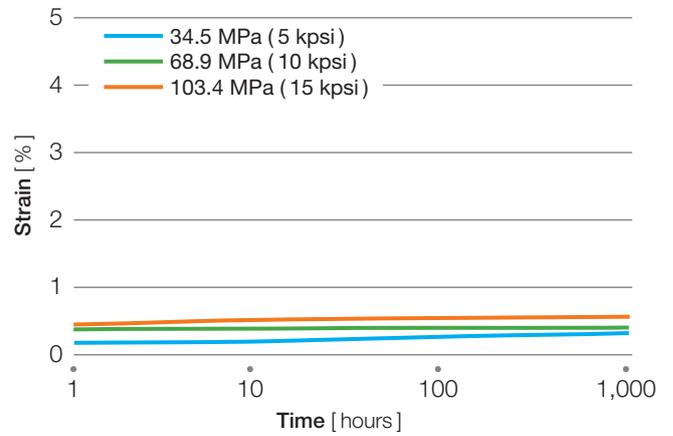


Figure 25: Torlon® 4203L strain vs. time at 204 °C (400 °F)

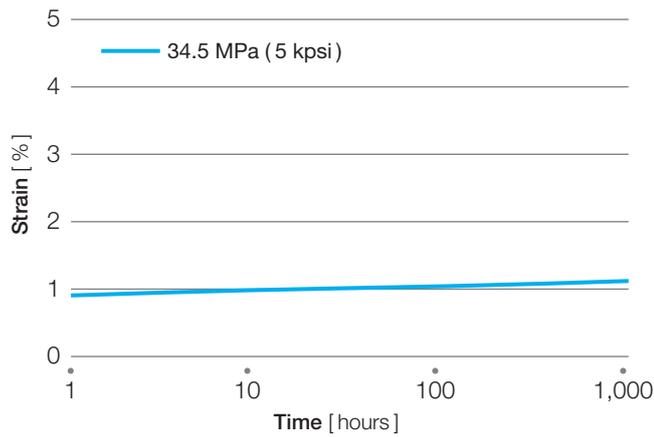


Figure 26: Torlon® 4275 strain vs. time at 204 °C (400 °F)

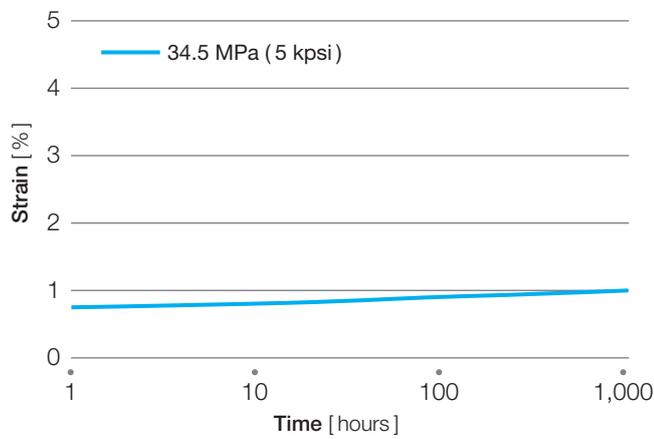


Figure 27: Torlon® 4301 strain vs. time at 204 °C (400 °F)

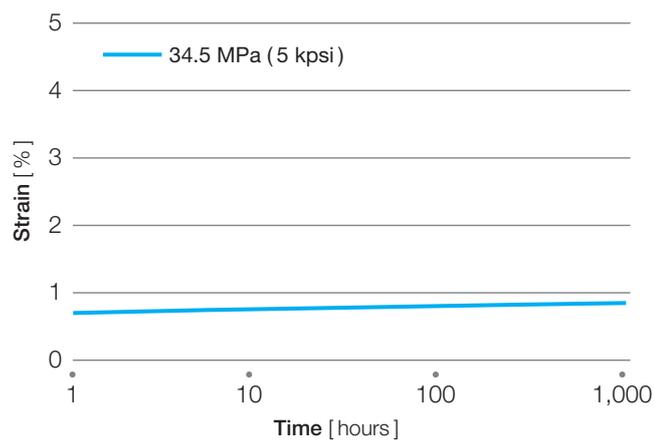


Figure 28: Torlon® 5030 strain vs. time at 204 °C (400 °F)

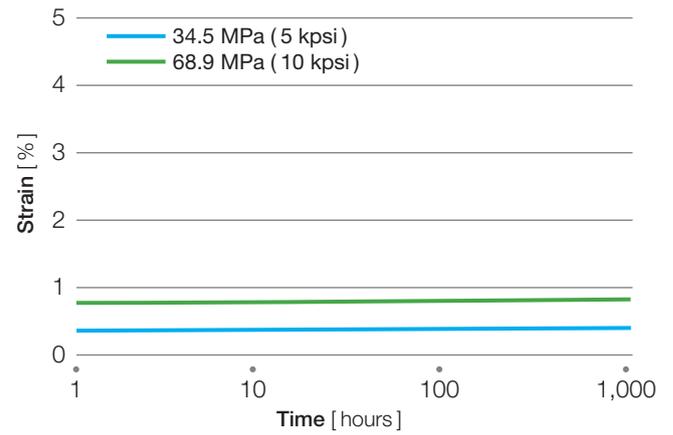
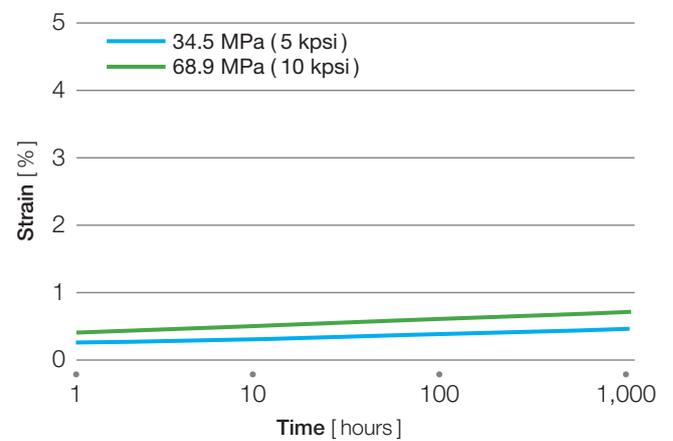


Figure 29: Torlon® 7130 strain vs. time at 204 °C (400 °F)



Flammability

Test data indicate the suitability of Torlon® PAI parts for electrical, electronic, aerospace, and other applications where flammability is of great concern. Torlon® 5030 and 7130 exceed FAA requirements for flammability, smoke density, and toxic gas emission; and they surpass, by a large margin, the proposed requirements for aircraft interior use.

Oxygen Index

The oxygen index is defined by ASTM D2863 as the minimum concentration of oxygen, expressed as volume percent, in a mixture of oxygen and nitrogen that will support flaming combustion of a material initially at room temperature under the conditions of this method.

Since ordinary air contains roughly 21 % oxygen, a material whose oxygen index is appreciably higher than 21 % is considered flame resistant because it will only burn in an oxygen-enriched atmosphere. The oxygen indices of several Torlon® PAI resins are shown in Table 15. The high values indicate a high degree of combustion resistance.

Table 15: Oxygen index per ASTM D2863

Grade	Oxygen Index [%]
4203L	45
4301	44
4275	45
5030	51
7130	52

NBS Smoke Density

When a material burns, smoke is generated. The quantity and density of the generated smoke is important in many applications.

ASTM E662 provides a standard technique for evaluating relative smoke density. This test was originally developed by the National Bureau of Standards (NBS) and is often referred to as the NBS Smoke Density test.

Torlon® PAI resins were tested using both the smoldering and flaming modes, following NFPA 258 procedures using 1.3 mm to 1.5 mm (0.05 inch to 0.06 inch) specimens. The results are shown in Table 16.

Table 16: NBS smoke density

Property	4203L		5030		7130	
	Sm ⁽¹⁾	Fl ⁽²⁾	Sm	Fl	Sm	Fl
Minimum light transmittance, %	92	6	96	56	95	28
Maximum specific optical density (D _m)	5	170	2	35	3	75
Time to 90% D _m , minutes	18.5	18.6	10.7	15.7	17.0	16.0

⁽¹⁾ Sm = Smoldering

⁽²⁾ Fl = Flaming

Toxic Gas Emission Test

Table 17: FAA toxic gas emission test

Chemical	5030		7130	
	Sm ⁽¹⁾	Fl ⁽²⁾	Sm	Fl
Hydrochloric acid	0	<1	0	<1
Hydrofluoric acid	0	0	0	0
Carbon monoxide	<10	120	<10	100
Nitrogen oxides	<2	19	0	14
Hydrocyanic acid	0	4	0	5
Sulfur dioxide	0	0	0	4

⁽¹⁾ Sm = Smoldering, ppm

⁽²⁾ Fl = Flaming, ppm

Ignition Properties

The ignition properties of Torlon® 4203L resin were measured using ASTM Test Method D1929 and the results are shown in Table 18.

Flash ignition temperature is defined as the lowest temperature of air passing around the specimen at which a sufficient amount of combustible gas is evolved to be ignited by a small external pilot flame.

Self-ignition temperature is defined as the lowest temperature of air passing around the specimen at which, in the absence of an ignition source, the self-heating properties of the specimen lead to ignition or ignition occurs of itself, as indicated by an explosion, flame, or sustained glow. These values can be used to rank materials according to their ignition susceptibility.

Table 18: Ignition properties of Torlon® 4203L

ASTM D1929	°C	°F
Flash ignition temperature	570	1,058
Self ignition temperature	620	1,148



UL 94 Flammability Standard

The UL 94 flammability standard established by Underwriters Laboratories is a system by which plastic materials can be classified with respect to their ability to withstand combustion. The flammability rating given to a plastic material is dependent upon the response of the material to heat and flame under controlled laboratory conditions and serves as a preliminary indicator of its acceptability with respect to flammability for a particular application. The actual response to heat and flame of a thermoplastic depends on other factors such as the size, form, and end-use of the product. Additionally, characteristics in end-use application such as ease of ignition, burning rate, flame spread, fuel contribution, intensity of burning, and products of combustion will affect the combustion response of the material.

Three primary test methods comprise the UL 94 standard. They are the *Horizontal Burning Test*, the *20 MM Vertical Burning Test*, and the *500 MW Vertical Burning Test*.

Horizontal burning test

For a HB classification rating, injection molded test specimens are limited to a 125 mm (5.0 inch) length, 13 mm (0.5 inch) width and the minimum thickness for which the rating is desired. The samples are clamped in a horizontal position with a 20 mm blue flame applied to the unclamped edge of the specimen at a 45° angle for 30 seconds or so, as soon as the combustion front reaches a pre-marked line 25 mm from the edge of the bar. After the flame is removed, the rate of burn for the combustion front to travel from the 25 mm line to a pre-marked 100 mm line is calculated. At least three specimens are tested in this manner. A plastic obtains a HB rating by not exceeding a burn rate of 40 mm/min for specimens having a thickness greater than 3 mm or 75 mm/min for bars less than 3 mm thick.

The rating is also extended to products that do not support combustion to the 100 mm reference mark.

Table 19: UL criteria for classifying materials

Criteria	V-0	V-1	V-2
Afterflame time for each individual specimen, (t_1 or t_2)	≤ 10s	≤ 30s	≤ 30s
Total afterflame time for any condition set ($t_1 + t_2$ for the 5 specimens)	≤ 50s	≤ 250s	≤ 250s
Afterflame plus afterglow time for each individual specimen after the second flame application ($t_2 + t_3$)	≤ 30s	≤ 60s	≤ 60s
Afterflame or afterglow of any specimen up to the holding clamp	No	No	No
Cotton indicator ignited by flaming particles or drops	No	No	Yes

20 mm vertical burn test

Materials can be classified V-0, V-1, or V-2 based on the results obtained from the combustion of samples clamped in a vertical position.

The 20 mm vertical burn test is more aggressive than the HB test and is performed on samples that measure 125 mm in length, 13 mm in width, and the minimum thickness at which the rating is desired (typically 0.8 mm or 1.57 mm).

The samples are clamped in a vertical position with a 20 mm high blue flame applied to the lower edge of the clamped specimen. The flame is applied for 10 seconds and removed. When the specimen stops burning, the flame is reapplied for an additional 10 seconds and then removed. A total of five bars are tested in this manner. Table 19 lists the criteria by which a material is classified in this test.

Table 20 gives the ratings of selected grades of Torlon® PAI resins. The most current ratings of Torlon® PAI resins can be found at the Underwriters Laboratories web site at www.ul.com.

Table 20: Vertical flammability by Underwriters Laboratories (UL 94)

Grade	Thickness		UL 94 Rating
	[mm]	[inch]	
4203, 4203L	1.2	0.047	V-0
	2.4	0.094	V-0
	3.0	0.118	V-0
4301	1.2	0.047	V-0
	2.4	0.094	V-0
	3.0	0.118	V-0
5030	1.2	0.047	V-0
	1.5	0.059	V-0
	2.4	0.094	V-0
	3.0	0.118	V-0



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FAA Flammability

Torlon® 5030 and 7130 were tested by the FAA vertical flammability test for Transport Category Airplanes as described in 25.853(a) and Appendix F. The results are shown in Table 21.

Samples of Torlon® 5030 and 7130 were also tested for horizontal flammability (FAA Transport Category Airplanes, 25.853 [b-3] and Appendix F) and 45 flammability (FAA Cargo and Baggage Compartment, 25.855 [1-a]). In both cases, the test specimens did not ignite. Based on that result, Torlon® 5030 and 7130 meet the requirements of these codes.

Table 21: FAA vertical flammability

Grade	Average Burn Length	
	[mm]	[inch]
5030	15.2	0.6
7130	15.2	0.6

UL 57 Electric Lighting Fixtures

Torlon® 4203L resin was tested for conformance to the flammability requirements of this standard. The results shown in Table 22 show that the requirements are met.

Note: The test methods used to obtain the data in this section measure response to heat and flame under controlled laboratory conditions detailed in the test method specified and may not provide an accurate measure of fire hazard under actual fire conditions. Furthermore, as Solvay has no control over final formulation by the user of these resins including components incorporated either internally or externally, nor over processing conditions or final physical form or shape, these results may not be directly applicable to the intended end use.

Table 22: Electric lighting fixtures, flammability requirements (UL 57)

Grade	Test Results
4203L	Noncombustible by section 81.12 for thickness of 1.02 mm, 3.18 mm and 5.08 mm (0.040 inch, 0.125 inch and 0.200 inch)

Performance in Various Environments

Chemical Resistance

Torlon® PAI is virtually unaffected by aliphatic and aromatic hydrocarbons, chlorinated and fluorinated hydrocarbons, and most acids at moderate temperatures. The polymer, however, may be attacked by saturated steam, strong bases, and some high-temperature acid systems. The effects of a number of specific chemicals on the tensile strength of Torlon® 4203L are presented in Table 23. Proper post-cure of Torlon® PAI parts is necessary to achieve optimal chemical resistance.

Table 23: Chemical resistance of Torlon® 4203L, 24 hr at 93 °C (200 °F)

Chemical	Rating
Acids	
Acetic acid (10%)	A
Glacial acetic acid	A
Acetic anhydride	A
Lactic acid	A
Benzene sulfonic acid	F
Chromic acid (10%)	A
Formic acid (88%)	C
Hydrochloric acid (10%)	A
Hydrochloric acid (37%)	A
Hydrofluoric acid (40%)	F
Phosphoric acid (35%)	A
Sulfuric acid (30%)	A
Bases	
Ammonium hydroxide (28%)	C
Sodium hydroxide (15%)	F
Sodium hydroxide (30%)	F
Aqueous solutions (10%)	
Aluminum sulfate	A
Ammonium chloride	A
Ammonium nitrate	A
Barium chloride	A
Bromine (saturated solution, 49 °C (120 °F))	A
Calcium chloride	A
Calcium nitrate	A
Ferric chloride	A
Magnesium chloride	A
Potassium permanganate	A
Sodium bicarbonate	A
Silver chloride	A
Sodium carbonate	A
Sodium chloride	A
Sodium chromate	A
Sodium hypochlorite	A
Sodium sulfate	
Sodium sulfide	
Sodium Sulfite	



Chemical	Rating
Alcohols	
2-Aminoethanol	F
n-amyl alcohol	A
n-butyl alcohol	A
Cyclohexanol	A
Ethylene glycol	A
Amines	
Aniline	A
n-Butyl amine	A
Dimethylaniline	A
Ethylene diamine	F
Morpholine	A
Pyridine	F
Aldehydes & ketones	
Acetophenone	A
Benzaldehyde	A
Cyclohexanone	A
Formaldehyde (37 %)	A
Furfural	C
Methyl ethyl ketone	A
Chlorinated organics	
Acetyl chloride, 49°C (120°F)	A
Benzyl chloride, 49°C (120°F)	A
Carbon tetrachloride	A
Chlorobenzene	A
2-Chloroethanol	A
Chloroform, 49°C (120°F)	A
Epichlorohydrin	A
Ethylene chloride	A
Esters	
Amyl acetate	A
Butyl acetate	A
Butyl phthalate	A
Ethyl acetate	A
Ethers	
Butyl ether	A
Cellosolve	A
P-Dioxane, 49°C (120°F)	A
Tetrahydrofuran	A
Hydrocarbons	
Cyclohexane	A
Diesel fuel	A
Gasoline, 49°C (120°F)	A
Heptane	A
Mineral oil	A
Motor oil	A
Stoddard solvent	A
Toluene	A

Chemical	Rating
Nitriles	
Acetonitrile	A
Benzonitrile	A
Nitro compounds	A
Nitrobenzene	A
Nitromethane	A
Miscellaneous	
Cresyldiphenyl phosphate	A
Sulfolane	A
Triphenyl- phosphite	A
Key to compatibility ratings	
<i>A = Excellent – no attack, negligible effect on mechanical properties</i>	
<i>B = Good – slight attack, small reduction in mechanical properties</i>	
<i>C = Fair – moderate attack, material will have limited life</i>	
<i>F = Poor – material will fail, decompose, or dissolve in a short time</i>	



Table 24: Property retention after immersion in automotive lubricating fluids at 149 °C (300 °F)

Lubricant	4203L		4275	
	Weight Change [%]	Flexural Strength Retained [%]	Weight Change [%]	Flexural Strength Retained [%]
Motor oil ⁽¹⁾	0.0	99.4	0.0	95.5
Transmission fluid ⁽²⁾	0.0	100.3	0.0	94.2
Gear lube ⁽³⁾	+0.2	102.7	+0.2	100.6

⁽¹⁾ Valvoline SAE 20W

⁽²⁾ Exxon 11933

⁽³⁾ Penzoil 80W-90

Resistance to automotive and aviation fluids

Of particular interest to aerospace and automotive engineers is the ability of a polymer to maintain its properties after exposure to commonly used fluids. Total immersion tests show Torlon® PAI is not affected by common lubricating fluids at 149 °C (300 °F), aircraft hydraulic fluid at low temperatures, and turbine oil, even under stress at elevated temperatures. At 135 °C (275 °F), aircraft hydraulic fluid reduces strength slightly. Tables 24 and 25 summarize the methods and results of specific fluid immersion tests.

Automotive lubricating fluids

ASTM D790 specimens were tested at room temperature after immersion in 149 °C (300 °F) lubricating fluids for one month. Torlon® 4203L and 4275 have excellent property retention under these conditions, as shown in Table 24.

In a separate experiment, Torlon® 4301 and Torlon® 4275 were exposed to 3 different versions of Ford automatic transmission fluid (ATF) for 1,500 hours at 150 °C (302 °F). After exposure, the tensile strength and flexural modulus was determined and compared to the values obtained before exposure. The results shown in Table 25 indicate excellent resistance to degradation by these fluids.

Table 25: Effect of Ford automatic transmission fluid after 1,500 hours at 150 °C (302 °F)

Fluid	Tensile Strength Retained [%]		Flex Modulus Retained [%]	
	4301	4275	4301	4275
1	87	95	97	93
2	89	88	93	96
3	85	97	94	92

Aircraft hydraulic fluid (Skydrol® 500B)

Torlon® PAI bearing grades 4301 and 4275 were immersed in aircraft hydraulic fluid for 41 days at –80 °C (–108 °F) and 135 °C (275 °F). The change in tensile properties is shown in Table 26.

Both Torlon® PAI grades were mildly affected by the fluid at 135 °C (275 °F), showing a loss in tensile strength of about 10 %. It is noteworthy that this loss was not a result of embrittlement as tensile elongation was maintained. Tests show Torlon® 4203L bar specimens resist cracking, softening, and breakage under high stress in aircraft hydraulic fluid. Low temperature testing showed no significant effect on either grade.

Table 26: Tensile strength after immersion in aircraft hydraulic fluid⁽¹⁾

Grade	Tensile Strength Retained [%]	Elongation Retained [%]
4301		
1,000 hours at 135 °C (275 °F)	89.6	94.1
1,000 hours at –80 °C (–108 °F)	94.0	95.8
4275		
1,000 hours at 135 °C (275 °F)	92.7	119.3
1,000 hours at –80 °C (–108 °F)	101.3	129.8

⁽¹⁾ Skydrol® 500B

Aircraft turbine oil, with and without stress

Torlon® PAI parts have exceptional resistance to Aeroshell® 500 turbine oil under stress at elevated temperatures. Turbine oil affects Torlon® 4203L and 7130 only slightly; after 100 hours of exposure under stress, 4203L maintains more than 80 % of its ultimate tensile strength at temperatures up to 204 °C (400 °F) without rupturing, and 7130, a graphite-fiber-reinforced grade, is even better, tolerating stress levels of 80 % of ultimate at temperatures up to 232 °C (450 °F).

In another test, without stress, essentially no change in the tensile strengths of Torlon® 4203L and 4301 was observed after 1,000 hours in Aeroshell® 500 at 150 °C (302 °F).



Chemical Resistance Under Stress

Torlon® PAI parts which had been thoroughly post-cured were tested for chemical resistance under stress. Test specimens, 127 x 13 x 3 mm (5 x 0.5 x 0.125 inch) were clamped over a fixture with a 127 mm (5.0 inch) radius curved surface. The test chemical was applied to the middle of each specimen for one minute. The application was repeated after one and two hours. Specimens were inspected after 24 hours for breakage, cracking, swelling, and softening.

Resistance to the following chemical environments was tested: aviation gasoline, turbine fuel (Jet A/A-1), hydraulic fluid, methyl ethyl ketone, methylene chloride, 1,1,1 trichloroethane, and toluene. None of the Torlon® PAI specimens showed any breakage, cracking, swelling, or softening.

Effects of Water

Like other high-temperature engineering resins and composites, Torlon® PAI parts absorb water, but the rate is slow and parts can be rapidly restored to original dimensions and properties by drying.

Absorption rate

Torlon® PAI must be exposed to high humidity for a long time to absorb a significant amount of water. The rate of absorption depends on polymer grade, temperature, humidity, and part geometry.

Figures 30 and 31 report results obtained with uniform bars 127 x 13 x 3 mm (5 x 0.5 x 0.125 inch). Water absorption is dependent on diffusion into the part and is inversely proportional to part thickness.

Figure 30: Water absorption of Torlon® PAI polymers at 23 °C (73 °F), 50 % RH

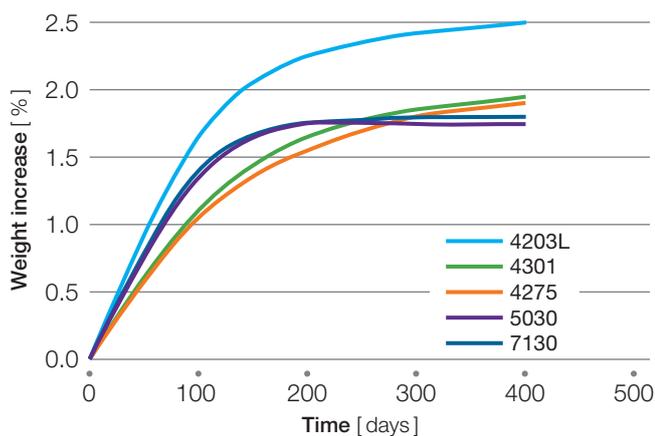


Figure 31: Water absorption of Torlon® PAI polymers at 43 °C (110 °F), 90 % RH

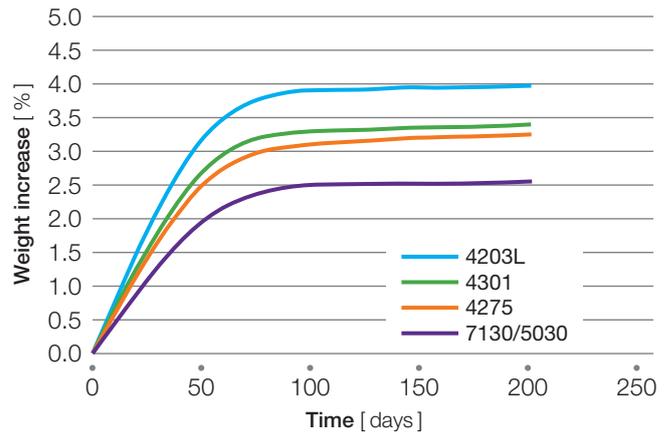
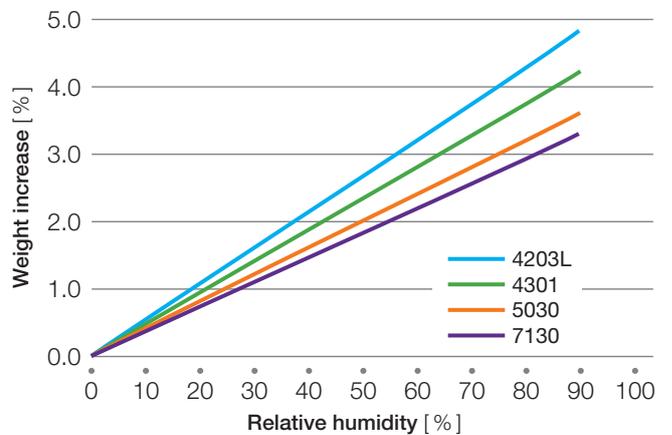


Figure 32: Equilibrium moisture absorption vs. relative humidity



Equilibrium absorption at constant humidity

At constant humidity, a Torlon® PAI part will absorb an equilibrium amount of water. The levels for a range of relative humidity are shown in Figure 32 using uniform panels whose dimensions were 127 x 13 x 3 mm (5 x 0.5 x 0.125 inch).

Dimensional changes

Small dimensional changes occur as Torlon® PAI parts absorb water. Figures 33 and 34 show dimensional changes of the standard test part with exposure to atmospheric moisture at specified temperatures. As with absorption rate, the change is greatest for Torlon® 4203L resin, the grade with least filler or reinforcement.

Restoration of dimensions and properties

Original dimensions and properties can be restored by drying Torlon® PAI parts. The temperature and time required depend on part size and geometry. For the test panels in this study, original dimensions were restored by heating for 16 hours at 149 °C (300 °F).



Changes in mechanical and electrical properties

To illustrate the change in mechanical properties with water absorption, test specimens were immersed in water until their weight increased by 2%. Table 27 compares the properties of these panels with those of panels conditioned for 40 hours at 23 °C (73 °F) and 50% relative humidity. A slight reduction in stiffness is the most noticeable change.

Absorbed water reduces the electrical resistance of Torlon® PAI resin and slightly changes dielectric properties. With 2% moisture, Torlon® PAI specimens had volume and surface resistivities of $3 \cdot 10^{14}$ ohm/m ($1 \cdot 10^{16}$ ohm/inch) and $1 \cdot 10^{17}$ ohm respectively, and dielectric strength of 24 kV/mm (620 V/mil).

Figure 33: Dimensional change of Torlon® PAI polymers at 23 °C (73 °F), 50% RH

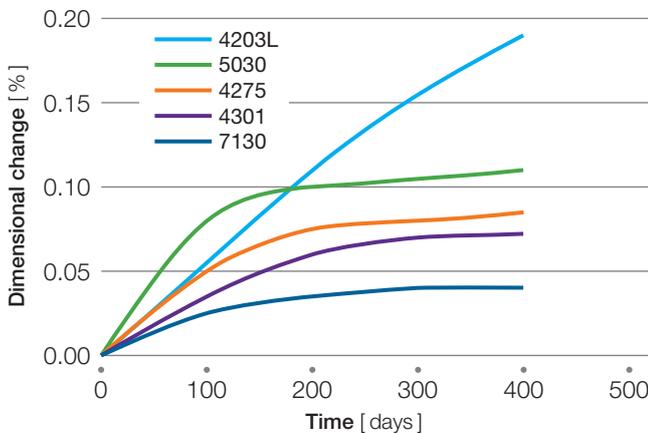


Figure 34: Dimensional change of Torlon® PAI polymers at 43 °C (110 °F), 90% RH

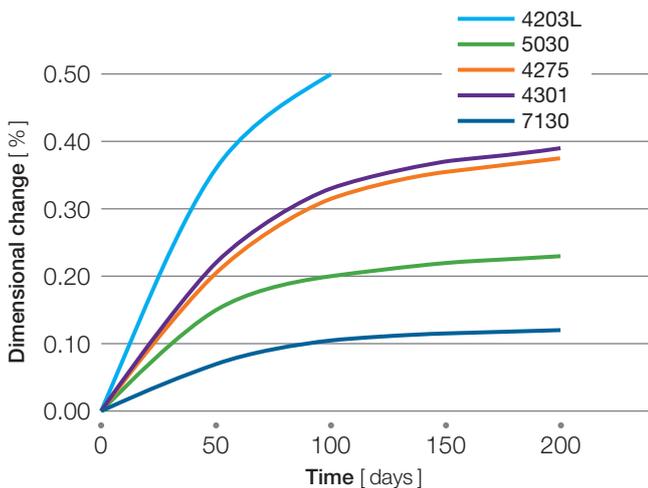


Table 27: Property change of Torlon® 4203L at 2% absorbed water

Property	Change [%]
Tensile strength	-7
Tensile modulus	-11
Elongation	13
Shear strength	1
Izod impact strength	20
Dielectric constant	18
Dissipation factor	53

Constraints on sudden high temperature exposure

Absorbed water limits the rate at which Torlon® PAI parts can be heated. Sudden exposure to high temperature can distort or blister parts unless absorbed water is allowed to diffuse from the part. Solvay uses the term “thermal shock temperature” to designate the temperature at which any distortion occurs upon sudden exposure to heat.

To determine the thermal shock temperature, test specimens 127 x 13 x 3 mm (5 x 0.5 x 0.12 inch) are exposed to 57.8% relative humidity and 23 °C (73 °F) over a specified period of time. The Torlon® PAI resin will absorb water. The amount absorbed will depend upon the exposure time and the grade of Torlon® PAI resin. The dimensions of the bars are measured and recorded.

The bars are then placed in a circulating air oven preheated to the test temperature. After one hour, the samples are removed, visually inspected, and measured. Failure occurs if blisters or bubbles appear or if dimensions increase by more than 0.025 mm (0.001 inch). The lowest temperature at which failure is seen is designated the thermal shock temperature.

Figure 35 relates thermal shock temperature to moisture content for Torlon® 4203L, the grade most sensitive to water absorption. At 2.5% absorbed water (which is equilibrium at 50% relative humidity and room temperature) the thermal shock temperature is well over 204 °C (400 °F). Thermal shock is related to exposure time in Figure 36. Even after over 200 hours at 57.8% relative humidity and 23 °C (73 °F), the test part made with Torlon® 4203L did not distort until sudden exposure to over 204 °C (400 °F). Other grades of Torlon® PAI resin exhibit lower equilibrium water absorption (refer to Figure 32 on page 23) and their thermal shock temperatures are therefore higher. Thermal shock temperature can be restored to its highest level by drying at 149 °C (300 °F) for 24 hours for each 3 mm (0.12 inch) of part thickness.



Figure 35: Thermal shock temperature vs. moisture content of Torlon® 4203L

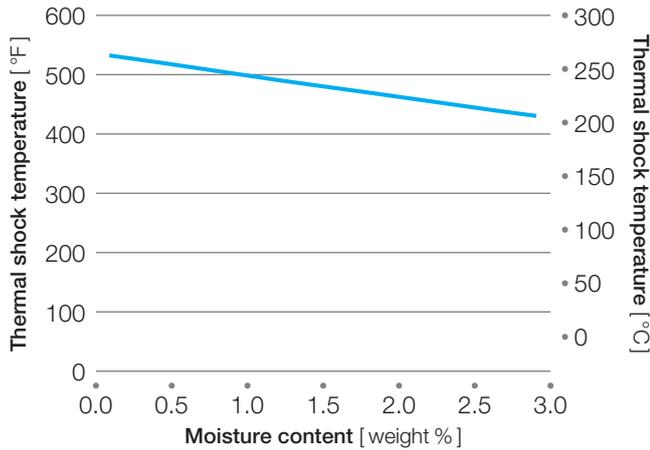


Figure 36: Thermal shock temperature vs. exposure time for Torlon® 4203L

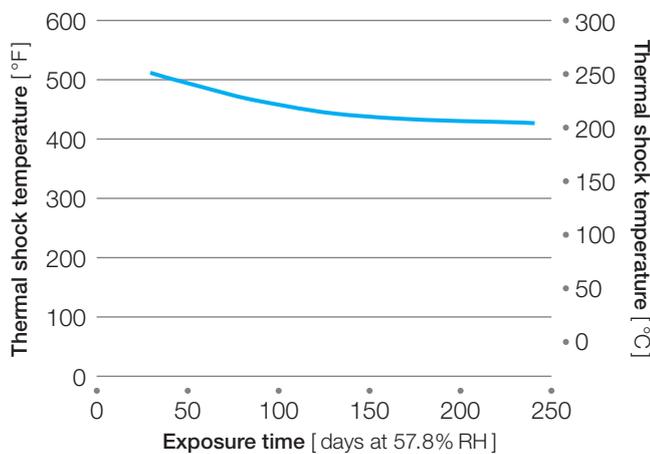
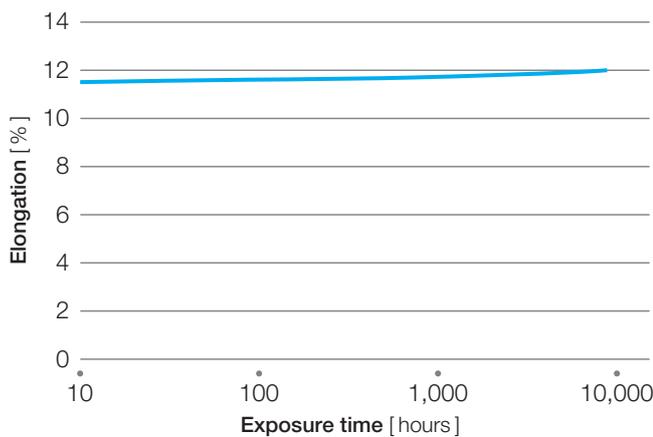


Figure 37: The elongation of Torlon® 4203L is essentially constant after exposure to simulated weathering



Weather-O-meter® Testing

Torlon® PAI molding polymers are exceptionally resistant to degradation by ultraviolet light. Torlon® 4203L resin did not degrade after 6,000 hours of Weather-O-meter® exposure (Figures 37 and 38) which is roughly equivalent to five years of outdoor exposure. The bearing grades, such as 4301, contain graphite powder which renders the material black and screens UV radiation. These grades are even more resistant to degradation from outdoor exposure.

Tensile bars conforming to ASTM test method D1708 were exposed in an Atlas Sunshine Carbon Arc Weather-O-meter®. Bars were removed after various exposure periods and tensile strength and elongation were determined. The test conditions were a black panel temperature of 63 °C (145 °F), 50 % relative humidity and an 18-minute water spray every 102 minutes.

Resistance to Gamma Radiation

Figure 39 shows the negligible effect gamma radiation has on Torlon® PAI – only about 5 % loss in tensile strength after exposure to 10⁹ rads.

Figure 38: Change in tensile strength of Torlon® 4203L with exposure to simulated weathering

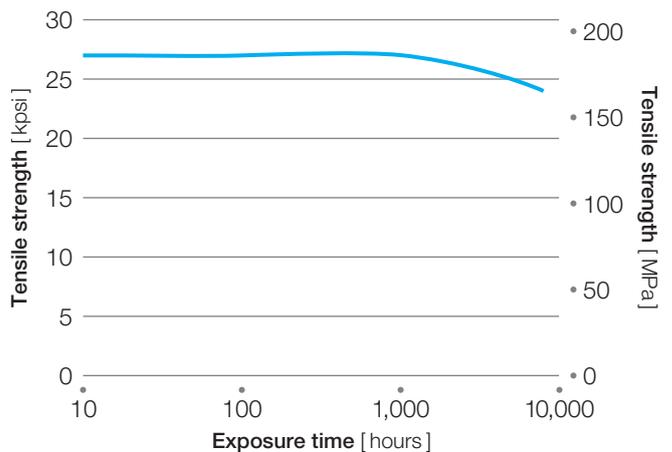
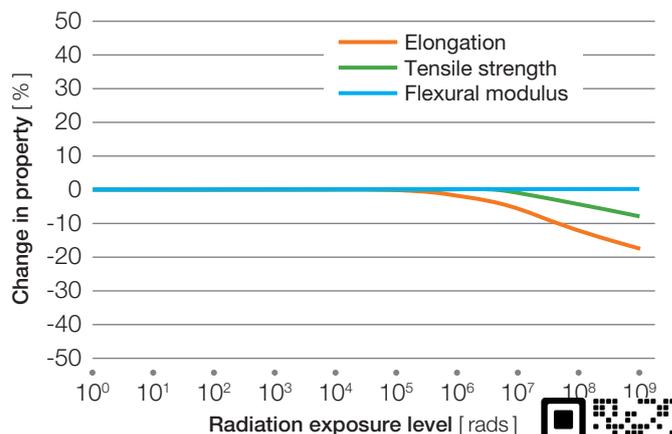


Figure 39: Property change of Torlon® 4203L due to gamma radiation



Electrical Properties

Most Torlon® PAI grades provide electrical insulation. Torlon® PAI provides a unique combination of high temperature service and ease of moldability into complex electrical and electronic parts. Special grades of Torlon® PAI engineering polymer are conductive. Torlon® 7130, a conductive grade, effectively shields electromagnetic interference. The design engineer should consider the significant electrical properties of a material, such as those summarized in Table 28.

Table 28: Important electrical considerations

Property	ASTM Test Method	Significance
Dielectric constant	D150	The ratio of the capacity of a condenser filled with the material to the capacity of an evacuated capacitor. It is a measure of the ability of the molecules to become polarized in an electric field. A low dielectric constant indicates low polarizability; thus the material can function as an insulator.
Dissipation factor	D150	A measure of the dielectric loss (energy dissipated) of alternating current to heat. A low dissipation factor indicates low dielectric loss, while a high dissipation factor indicates high loss of power to the material, which may become hot in use at high frequencies.
Volume resistivity	D257	The electrical resistance of a unit cube calculated by multiplying the resistance in ohms between the faces of the cube by the area of the faces. The higher the volume resistivity, the better the material will function as an insulator.
Surface resistivity	D257	The resistance to electric current along the surface of a one square centimeter sample of material. Higher surface resistivity indicates better insulating properties.
Dielectric strength	D149	A measure of the voltage an insulating material can take before failure (dielectric breakdown). A high dielectric strength indicates the material is a good insulator.

Torlon® PAI Polymers for Insulating

Torlon® PAI resin has excellent electrical insulating properties and maintains them in a variety of environments. Torlon® PAI grades 4203L and 5030 have high dielectric strengths and high volume and surface resistivity as shown in Table 29.

The Torlon® PAI grades intended for wear-resistant applications – 4301, 4275, and 4435 – contain graphite which under some conditions can conduct electricity. Although these materials have high resistivities by the ASTM test method D257, which uses direct current for its measurements, these materials may demonstrate some conductivity at higher frequencies and voltages.

Table 29: Electrical properties of Torlon® PAI resins

	Grade				
	4203L	4301 ⁽¹⁾	4275 ⁽¹⁾	4435 ⁽¹⁾	5030
Volume resistivity (ASTM D257)					
ohm·cm	2·10 ¹⁷	8·10 ¹⁵	8·10 ¹⁵	2·10 ⁷	2·10 ¹⁷
Surface resistivity (ASTM D257)					
ohm	5·10 ¹⁸	8·10 ¹⁷	4·10 ¹⁷	6·10 ¹⁰	1·10 ¹⁸
Dielectric strength [1 mm (0.040 inch)] (ASTM D149)					
V/mil	580				840
kV/mm	24				33
Dielectric constant (ASTM D150)					
10 ³ Hz	4.2	6.0	7.3	4.4	
10 ⁶ Hz	3.9	5.4	6.6	4.2	
Dissipation factor (ASTM D150)					
10 ³ Hz	0.026	0.037	0.059	0.022	
10 ⁶ Hz	0.031	0.042	0.063	0.023	

⁽¹⁾ Contains graphite powder. By these tests, they behave as insulators, but they may behave in a more conductive manner at high voltage or high frequency.



Service in Wear-Resistant Applications

An Introduction to Torlon® PAI Wear-Resistant Grades

New possibilities in the design of moving parts are made available by Torlon® PAI wear-resistant grades: 4301, 4275, and 4435. These materials offer high compressive strength and modulus, excellent creep resistance, and outstanding retention of strength and modulus at elevated temperatures, as well as self-lubricity and low coefficients of thermal expansion, which make them prime candidates for wear surfaces in severe service. Torlon® PAI bearings are dependable in lubricated, unlubricated, and marginally lubricated service. Some typical applications which lend themselves to this unique set of properties are plain bearings, thrust washers, seal rings, vanes, valve seats, bushings, and wear pads.

Bearing Design Concepts

Whenever two solids rub against each other, some wear is inevitable. The force pressing the sliding surfaces together (pressure) and the speed at which the sliding occurs (velocity) impact the rate at which wear occurs.

Wear rate relationship

The rate at which wear occurs can be related to the pressure and velocity by the following empirical equation:

$$t = KPVT$$

where:

t = wear

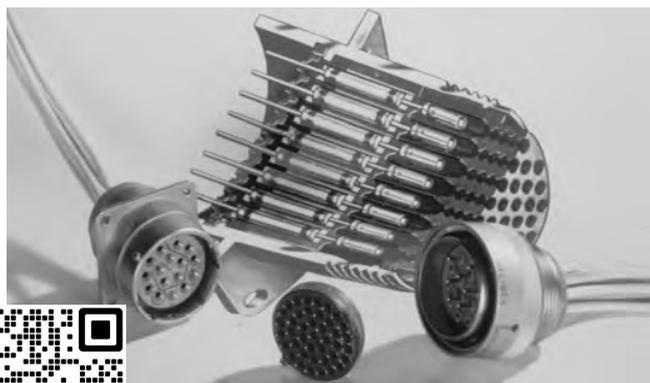
K = wear factor determined at a given P and V

P = pressure on bearing surface

V = bearing surface velocity

T = time

This equation seems to suggest that the wear will be directly proportional to the pressure and velocity. That would be true if the wear factor K were constant. For polymeric materials, the wear factor is not constant and varies with the pressure and velocity. The equation is only useful for calculating the wear depth at a particular PV from the wear rate at that PV and the expected service life, corrected for duty factor.



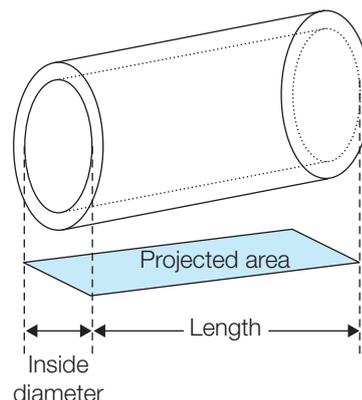
Calculating the pressure and velocity

Bearings

A typical plain bearing application consists of a sleeve bearing around a rotating shaft. To calculate the sliding velocity in meters per minute, multiply the shaft diameter in millimeters by the rpm, then by 0.003144; or to get the velocity in feet per minute, multiply the shaft diameter in inches by the revolutions per minute (rpm), and then by 0.262. For example, a 12.7 mm shaft rotating at 1,200 rpm, would have a velocity of 47.9 meters per minute or (dividing by 60) 0.8 meters per second. Or in US customary units, the 0.5 inch shaft rotating at 1,200 rpm would have a velocity of 157.2 feet per minute.

To calculate the pressure, divide the total load by the area. For sleeve bearings, the projected area is typically used, so the length of the sleeve would be multiplied by the inside diameter of the bearing as shown in Figure 40. In the SI system, pressure is usually expressed in Pascals, which is the same as Newtons per square meter. In US customary units, the pressure is expressed in pounds per square inch.

Figure 40: Calculating bearing projected area



Thrust washers

To calculate the sliding velocity of a thrust washer application, the mean diameter is typically used to determine the length per revolution. For example, a thrust washer with an outside diameter of 76 mm (3 inch) and an inside diameter of 51 mm (2 inch), would have a mean diameter of 63.5 mm (2.5 inch), and the distance slid per revolution would be obtained by multiplying that diameter by π or 3.14. That value would be multiplied by the rpm and, in the SI system, divided by 60,000 to get velocity in meters per second. In the US system, the mean diameter in inches would be multiplied by 3.14 and the rpm, and then divided by 12 to get velocity in feet per minute. To continue the example, assume an rpm of 100, then the velocity in SI units is $63.5 \times 3.14 \times 100 \div 60,000$, or 0.33 meters per second. In US units, the velocity would be $2.5 \times 3.14 \times 100 \div 12$, or 65.4 feet per minute.



Design Guide



To calculate the pressure, the total load is divided by the bearing area. Figure 41 depicts the thrust washer used for this example and details the calculation of the bearing area. If the load on the washer is 444.8 Newtons (100 pounds), the pressure would be 444.8 N divided by 0.002531 m². In the US customary system, the pressure would be obtained by dividing the 100 divided by 3.925 or 25.47 psi. The result (175,740.8) would have units of N/m², which is defined as the Pascal (Pa). Dividing this value by 10⁶ gives a value of 0.1757 MPa.

For this example, the PV would be 0.058 MPa·m/s or 1,666 ft·lb/in²min.

PV limit concept

Either increasing the pressure or the velocity will cause added friction and subsequently additional frictional heat. Because the properties of polymeric materials vary with temperature, the product of the pressure and velocity is useful for predicting the performance of a polymeric bearing material. If a polymeric bearing material is tested at varying pressures and velocities, and the results related to the pressure-velocity product (PV), the behavior shown in Figure 42 is typical. At low to moderate PV's, wear is low. As the PV is increased, at some point the wear becomes rapid. The PV at which this transition occurs is commonly called the PV limit or limiting PV. Due to heat of friction, bearings in service above the PV limit of the material wear very rapidly and may actually melt.

Figure 41: Thrust washer calculation example

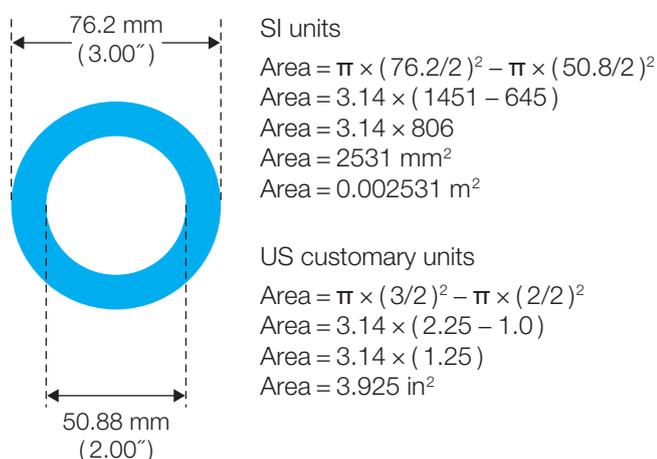
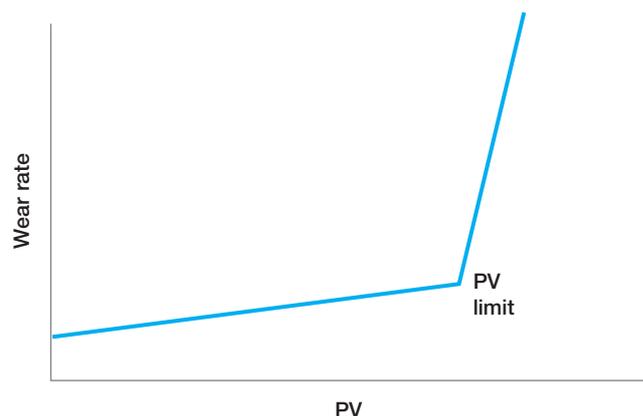


Figure 42: Material wear rate is a function of the pressure-velocity (PV) product



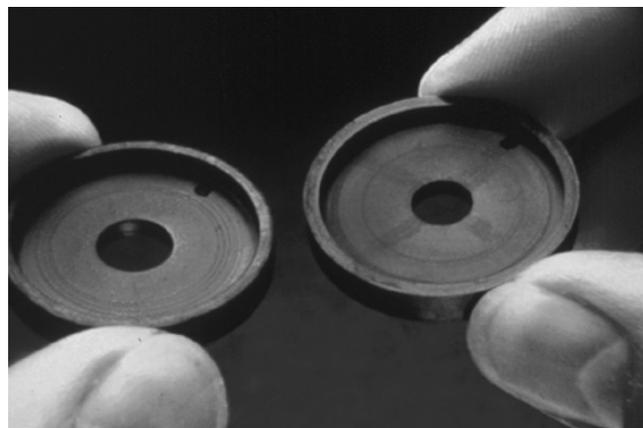
Measuring wear resistance

There are a variety of methods for evaluating relative wear resistance. Because of the large number of independent variables, there is little correlation between methods.

The method used for the wear resistance data in this document was ASTM D3702, using a manual thrust bearing, 3-pin machine. The test specimens were prepared by injection molding a disc and machining it to the final configuration shown in Figure 43.

The samples were tested against a stationary washer made of AISI C-1018 steel having a surface finish of 0.4 μm (16 μinch). Testing was performed at ambient temperature and humidity without any external lubrication. Thrust washer specimens were broken in to remove any surface irregularities at a velocity of 60m/min (200 ft/min) and a pressure of 8.5 bar (125 psi) for a period of 20 hours. Then each sample was tested at the specified velocity and pressure for 20 hours. Height measurements were taken before and after at four equidistant points on the thrust washer disk and the average wear depth in mm (in inches) was reported and used in the calculation of the wear factor.

Figure 43: Thrust washer test specimen



Torlon® PAI Wear-Resistant Grades

Low wear factors (K) are characteristic of wear resistant materials. Fluoropolymers, which have low coefficients of friction, have very low wear factors, but limited mechanical properties and poor creep resistance. At low PV's, Torlon® PAI wear resistant grades have wear factors comparable to filled polytetrafluoroethylene (PTFE), a fluoropolymer, but Torlon® PAI polymers offer superior creep resistance and strength.

Torlon® PAI polymers have wear factors similar to those of more expensive polyimide resins, and there is a distinct cost advantage in choosing Torlon® PAI. In addition, Torlon® PAI resins are injection moldable; polyimides are not.

The wear factors and coefficient of friction obtained when wear resistant grades of Torlon® PAI were tested at various PV's are shown in Table 30.

Table 30: Wear factor and coefficient of friction, dry environment

P [MPs (psi)]	PV [MPa·m/s (psi·ft/min)]	Grade					
		4301		4275		4630	
		WF ⁽¹⁾	COF ⁽²⁾	WF	COF	WF	COF
Velocity – 0.25 m/s (50 ft/min)							
3.4 (500)	0.9 (25,000)	28.2 (14.0)	0.31	26.2 (13.0)	0.31	12.1 (6.0)	0.32
6.9 (1,000)	1.7 (50,000)	33.2 (16.5)	0.27	32.2 (16.0)	0.27	36.3 (18.0)	0.29
10.3 (1,500)	2.6 (75,000)	30.2 (15.0)	0.24	34.8 (17.3)	0.24	28.6 (14.2)	0.20
13.8 (2,000)	3.4 (100,000)	55.4 (27.5)	0.19	45.1 (22.4)	0.18	30.8 (15.3)	0.13
17.2 (2,500)	4.3 (125,000)	66.9 (33.2)	0.15	33.8 (16.8)	0.14	24.6 (12.2)	0.11
20.7 (3,000)	5.2 (150,000)	NT ⁽³⁾	NT	30.6 (15.2)	0.12	22.6 (11.2)	0.10
Velocity – 1 m/s (200 ft/min)							
0.9 (125)	0.9 (25,000)	38.3 (19.0)	0.35	NT	NT	NT	NT
1.7 (250)	1.7 (50,000)	31.2 (15.5)	0.35	34.2 (17.0)	0.31	30.2 (15.0)	0.32
2.6 (375)	2.6 (75,000)	191.0 (94.8)	0.25	58.4 (29.0)	0.24	44.3 (22.0)	0.19
3.4 (500)	3.4 (100,000)	NT	NT	111.4 (55.3)	0.18	44.7 (22.2)	0.17
4.3 (625)	4.3 (125,000)	NT	NT	100.3 (49.8)	0.18	36.9 (18.3)	0.14
5.2 (750)	5.2 (150,000)	NT	NT	558.0 (277.0)	0.14	36.3 (18.0)	0.12
Velocity – 4 m/s (800 ft/min)							
0.2 (31.25)	0.9 (25,000)	34.2 (17.0)	0.39	35.3 (17.5)	0.29	27.2 (13.5)	0.32
0.4 (62.5)	1.7 (50,000)	77.6 (38.5)	0.28	40.3 (20.0)	0.34	47.3 (23.5)	0.24
0.6 (93.75)	2.6 (75,000)	73.1 (36.3)	0.21	75.1 (37.3)	0.21	37.7 (18.7)	0.22
0.9 (125)	3.4 (100,000)	151.1 (75.0)	0.24	199.8 (99.2)	0.16	48.3 (24.0)	0.16
1.1 (162.5)	4.5 (125,000)	239.7 (119.0)	0.22	151.5 (75.2)	0.21	68.5 (34.0)	0.14
1.3 (187.5)	5.2 (150,000)	NT	NT	NT	NT	96.7 (48.0)	0.14

⁽¹⁾ WF = Wear Factor of $10^{-8} \text{ mm}^3/\text{N} \cdot \text{m}$ ($10^{-10} \text{ in}^3/\text{min}/\text{ft} \cdot \text{lb} \cdot \text{hr}$), ⁽²⁾ COF = Coefficient of Friction, ⁽³⁾ NT = Not Tested



Effect of Mating Surface on Wear Rate

The wear data presented in Table 31 was determined using C1018 steel hardened to 24 on the Rockwell C scale. Various metals were tested against Torlon® 4301 to evaluate the effect of the mating surface on wear resistance.

Lubricated Wear Resistance

The impressive performance of Torlon® PAI bearing grades in dry (non-lubricated) environments is insurance against catastrophic part failure or seizure upon lube loss in a normally lubricated environment. In a transmission lubricated with hydrocarbon fluid, Torlon® PAI thrust washers are performing well at PVs of 45.54 MPa·m/s (1,300,000 ft·lbs/in²·min). In a water-lubricated hydraulic motor vane, excellent performance has been attained at over 2,000,000 PV (70.05 MPa·m/s). Table 32 summarizes the wear characteristics of Torlon® 4301 immersed in hydraulic fluid.

Table 33 shows the wear factor and coefficient of friction of various wear-resistant grades of Torlon® PAI resin in lubricated conditions.

Table 31: Wear characteristics of Torlon® 4301 against various metals

Metal used as mating surface for Torlon® 4301

C1018 (Standard)	C1018 Soft	316 Stainless Steel	Aluminum Die Casting Alloys		
			Brass	A360	A380
Rockwell hardness, C scale					
24	6	17	-15	-24	-28
Relative wear factor at high velocity					
1.0	1.4	7.5	2.1	1.3	1.2
Relative wear factor at low velocity					
1.0	1.2	1.2	1.5	1.5	0.9

Table 32: Lubricated wear resistance of Torlon® 4301

PV (P/V = 50/900)	45,000
Wear factor, K (10 ⁻¹⁰ in ³ ·min/ft·lb·hr (10 ⁻⁸ mm ³ /N·m))	1.0 (2.1)
Coefficient of friction, static	0.08
Coefficient of friction, kinetic	0.10
Wear depth at 1,000 hours, mm (inch)	0.11 (0.0045)

Table 33: Wear factor and coefficient of friction, lubricated environment

P [MPa (psi)]	V [m/s (ft/min)]	PV [MPa·m/s (psi·ft/min)]	Grade							
			4301		4275		4630		4645	
			WF ⁽¹⁾	COF ⁽²⁾	WF	COF	WF	COF	WF	COF
6.9 (1,000)	25 (75)	1.7 (75,000)	18.1 (9.0)	0.18	14.1 (7.0)	0.15	22.2 (11.0)	0.15	3.2 (1.6)	0.09
5.2 (750)	4 (800)	20.7 (600,000)	0.7 (0.4)	0.03	1.3 (0.7)	0.05	2.0 (1.0)	0.03	0.7 (0.3)	0.07

⁽¹⁾ WF = Wear Factor of 10⁻⁸ mm³/N·m (10⁻¹⁰ in³min/ft·lb·hr), ⁽²⁾ COF = Coefficient of Friction



Wear Resistance and Post-Cure

The wear resistance of Torlon® PAI parts depends on proper post-cure. A thorough and complete post-cure is necessary to achieve maximum wear resistance. To illustrate the dependence of wear resistance on post-cure, a sample of Torlon® 4301 was post-cured through a specified cycle and tested for wear resistance at various points in time. The results of that test and the cure cycle are shown in Figure 44. In this case, the Wear Factor, K, reached a minimum after 11 days, indicating achievement of maximum wear resistance.

The length of post-cure will depend on part configuration, thickness, and to some extent on molding conditions. Very long exposure to 260 °C (500 °F) is not detrimental to Torlon® PAI parts. The suitability of shorter cycles must be verified experimentally.

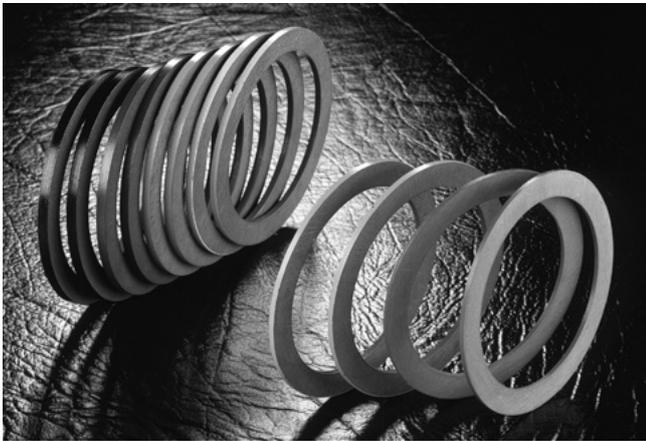
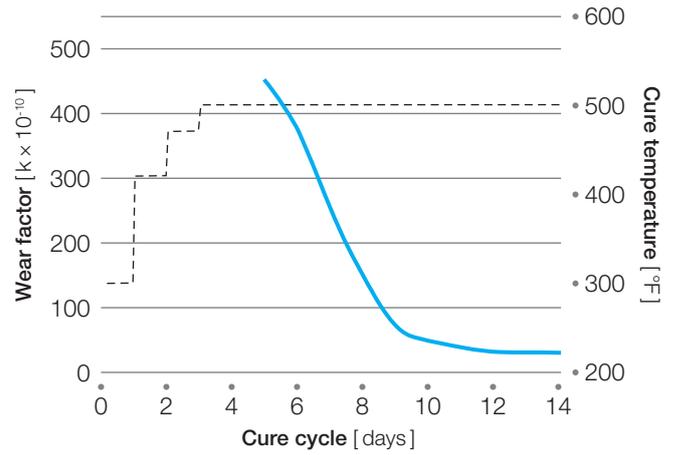


Figure 44: Extended cure at 260 °C (500 °F) improves wear resistance



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Bearing Design

When designing a bearing to be made of Torlon® PAI, it is important to remember that adequate shaft clearance is critical. With metal bearings, high clearances tend to result in shaft vibration and scoring. PAI bearings are much more resilient, dampen vibrations, and resist scoring or galling. The bearing inside diameter will be determined by adding the total running clearance to the shaft outside diameter. The total running clearance is the total of the basic clearance, the adjustment for high ambient temperature, and an adjustment for press fit interference if the bearing is press fit.

Figure 45 shows the basic clearance as a function of shaft diameter. If the bearing is to be used at ambient temperatures greater than room temperature, then the factor shown in Figure 46 should be applied. Figure 47 gives the recommended allowance for using a press fit bearing.

To give an example of how to properly size a PAI bearing, consider this hypothetical situation with a shaft diameter of 51 mm (2 inch) and bearing wall thickness of 5 mm (0.2 inch) to operate at an ambient temperature of 65 °C (150 °F). The PAI bearing is to be press fit into a steel housing. The basic clearance from Figure 45 is 9 mils or 0.23 mm (0.009 inch).

The additional clearance for the elevated ambient temperature is obtained by multiplying the factor from Figure 46 (0.0085) by the wall thickness to obtain 0.04 mm (0.0017 inch). The recommended interference for the press fit is 0.13 mm (0.005 inch). Because the inside diameter of the bearing will be decreased by the amount of the interference, that amount is added to the clearance. Therefore the total clearance will be the basic clearance 0.23 mm (0.009 inch) plus the temperature clearance 0.04 mm (0.0017 inch) plus the interference 0.13 mm (0.005 inch) to give 0.40 mm (0.0157 inch). Therefore the inside diameter of the PAI bearing should be 51.2 mm (2.0157 inch).

Figure 45: Basic bearing shaft clearance

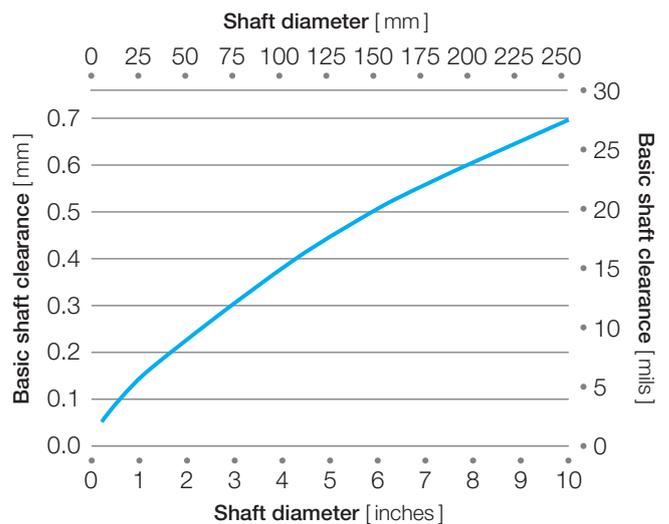


Figure 46: Clearance factor for elevated ambient temperature

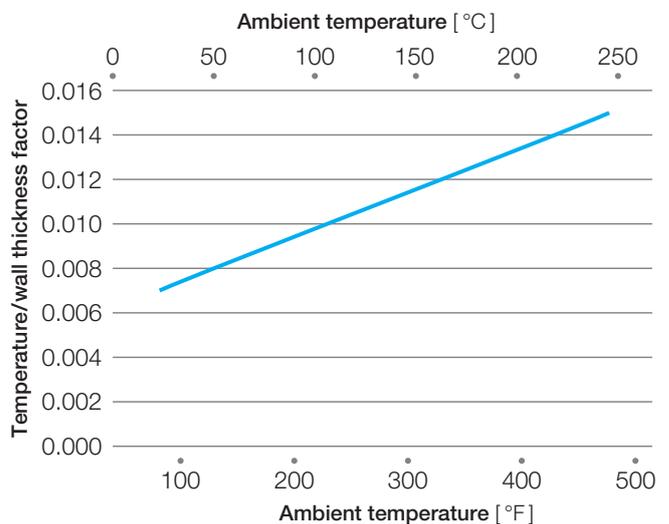
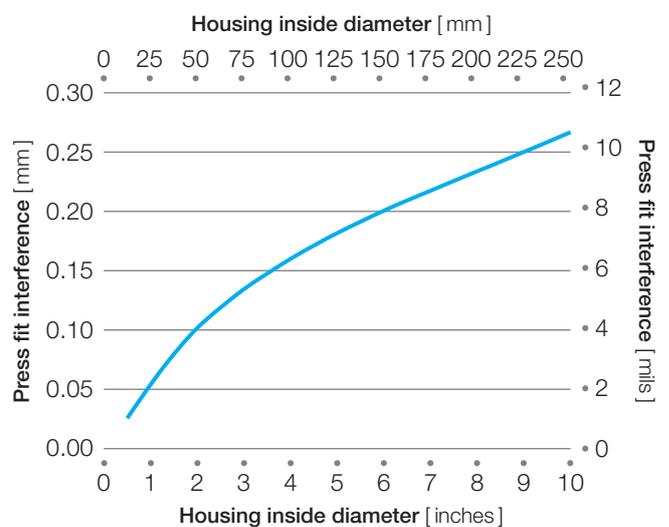


Figure 47: Press fit interference



Industry and Agency Approvals

Torlon® PAI polymers have been tested successfully against many industry standards and specifications. The following list is a summary of approvals to date, but should not be considered inclusive, as work continues to qualify Torlon® PAI for a myriad of applications.

ASTM D5204 Standard Classification System for Polyamide-imide (PAI) Molding and Extrusion Materials

Grade	ASTM D5204 Designation
4203L	PAI000R03A56316E11FB41 or PAI011M03 or PAI021M03
4301	PAI000L15A32232E12FB42 or PAI012L15 or PAI022L15
4275	PAI000L23A22133E13FB42 or PAI012L23 or PAI022L23
4435	PAI0120R35 or PAI0220R35
4630	PAI0120R30 or PAI0220R30
4645	PAI0120R45 or PAI0220R45
5030	PAI000G30A61643E15FB46 or PAI013G30 or PAI023G30
7130	PAI000C30A51661FB47 or PAI013C30 or PAI023C30

Federal Aviation Administration

Torlon® 5030 and 7130 pass FAA requirements for flammability, smoke density, and toxic gas emissions.

Military Specification MIL-P-46179A

This specification was cancelled on July 27, 1994 and ASTM D5204 was adopted by the Department of Defense. The following cross reference table appears in the adoption notice.

Type	Class	ASTM D5204
4203L	I	PAI000R03A56316E11FB41
4301	II	1 PAI000L15A32232E12FB42
4275	II	2 PAI000L23A22133E13FB42
5030	III	1 PAI000G30A61643E15FB46
7130	IV	PAI000C30A51661FB47

National Aeronautics and Space Administration

NHB8060.1 “Flammability, Odor, and Offgassing Requirements and Test Procedures for Materials in Environments that Support Combustion” Torlon® 4203L and 4301 have passed the NASA spacecraft materials requirements for non-vacuum exposures per NHB8060.1.

Society of Automotive Engineers-Aerospace Material Specifications

AMS 3670 is the specification for Torlon® PAI materials. The specification suggests applications requiring a low coefficient of friction, thermal stability, and toughness up to 250 °C (482 °F). Torlon® 4203L, 4275, 4301, 5030, and 7130 are covered in the detail specifications:

AMS 3670/1-Torlon® 4203L
AMS 3670/2-Torlon® 4275
AMS 3670/3-Torlon® 4301
AMS 3670/4-Torlon® 5030
AMS 3670/5-Torlon® 7130

Underwriters Laboratories

Vertical flammability

All Torlon® PAI grades have been awarded a V-0 classification. See Table 19 on page 20.

Continuous use

The Relative Thermal Indices of Torlon® 4203L, 4301, and 5030 are shown in Table 10 on page 14.



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Material Efficiency Specific Strength and Modulus

Reducing weight can be the key to lower cost, reduced friction, and decreased energy consumption. When a Torlon® PAI engineering polymer replaces metal, the Torlon® PAI part can support an equivalent load at significantly lower weight.

The ratio of a material's tensile strength to its density (specific strength) provides information about "material efficiency" The specific strength of Torlon® 5030, for example, is 1.3×10^5 J/kg (5.1×10^5 in·lbf/lb) compared with 0.8×10^5 J/kg (3.1×10^5 in·lbf/lb) for stainless steel. Therefore, a Torlon® 5030 part will weigh almost 40% less than a stainless steel part of equivalent strength. Similarly, the specific modulus of a material is of interest when stiffness of the part is crucial to performance.

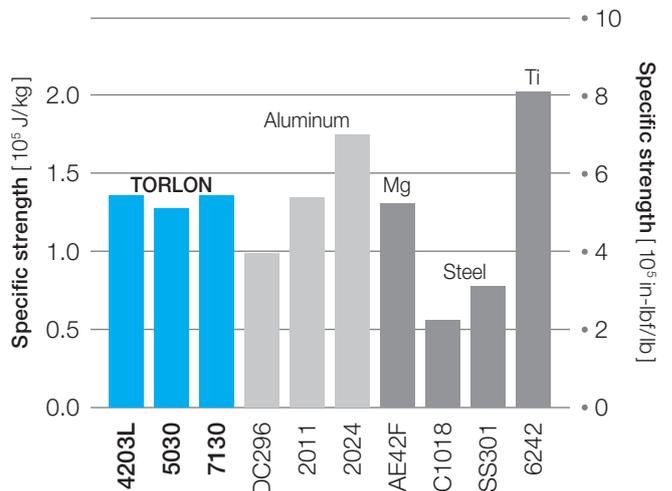
Comparison of material efficiency data in Table 34 and Figure 48 shows that Torlon® PAI can beat the weight of many metal parts.



Table 34: Specific strength and modulus of Torlon® PAI polymers and selected metals

Grade	Specific Strength		Specific Stiffness	
	[10^5 J/kg]	[10^5 in·lbf/lb]	[10^6 J/kg]	[10^7 in·lbf/lb]
4203L	1.4	5.5	3.4	1.4
5030	1.3	5.1	6.7	2.7
7130	1.4	5.4	15.0	6.0
Aluminum alloys, heat treated				
Die casting, A380	1.0	3.9	26.0	11.0
2011	1.3	5.4	25.0	10.0
2024	1.7	7.0	26.0	11.0
Magnesium AE42-F	1.3	5.2	25.0	9.8
Carbon steel, C1018	0.6	2.2	24.0	9.7
Stainless steel, 301	0.8	3.1	24.0	9.7
Titanium 6-2-4-2	8.1	2.0	26.0	10.0

Figure 48: Specific strength of Torlon® PAI resins vs. metal



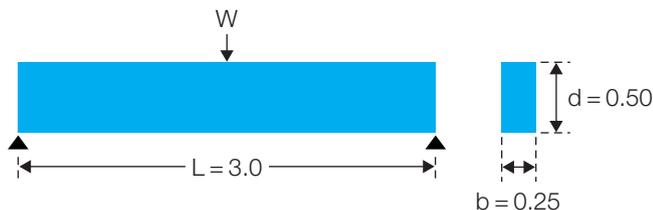
Geometry and Load Considerations

In the early stages of part design, standard stress and deflection formulas should be applied to ensure maximum working stresses do not exceed recommended limits.

Examples of Stress and Deflection Formula Application

Recommended maximum working stresses for Torlon® PAI polymers appear in Table 35 on page 37. To illustrate how these values may be used, the maximum load for a beam made of Torlon® 5030 will be calculated under various loading conditions at room temperature. Figure 49 shows the beam dimensions and the calculation of the moment of inertia (I).

Figure 49: Beam used in examples



W = Load, lb

L = Length of beam between supports, in

c = Distance from the outermost point in tension to the neutral axis, in

b = Beam width, in

d = Beam height, in

I = Moment of inertia, in⁴

In this example:

L = 3.0 in

c = 0.25 in

b = 0.25 in

d = 0.50 in

$$I = \frac{bd^3}{12} = \frac{(0.25 \text{ in})(0.50 \text{ in})^3}{12} = 0.0026 \text{ in}^4$$

Example 1 – Short-term loading

The maximum bending stress, S_{\max} , occurs at

$$L/2 \text{ and } M = \frac{WL}{4}$$

$$S_{\max} = \frac{WLC}{4I}$$

Solving for W and substituting the recommended maximum working stress for Torlon® 5030 under a short-term load at room temperature:

$$W_{\max} = \frac{4S_{\max}I}{Lc} = \frac{(4)(17,800 \text{ psi})(0.0026 \text{ in}^4)}{(3.0 \text{ in})(0.25 \text{ in})} = 247 \text{ lb}$$

Therefore, the maximum short-term load for a Torlon® 5030 beam at room temperature is approximately 59 kg. The maximum deflection for this beam is:

$$Y_{\max} = \frac{WL^3}{48EI} \text{ at } \frac{L}{2}$$

Where E is the flexural modulus of Torlon® 5030 obtained from Table 3.

$$Y_{\max} = \frac{(247 \text{ lb})(3.0 \text{ in})^3}{(48)(15.6 \times 10^5 \text{ psi})(0.0026 \text{ in}^4)} = 0.034 \text{ in}$$

Therefore, the predicted maximum deflection is 0.93 mm.

Example 2 – Steady load

In this example, the load is long-term. Creep is considered to be the limiting factor. The maximum load which may be applied to the Torlon® 5030 beam is:

$$W_{\max} = \frac{4S_{\max}I}{Lc} = \frac{(4)(17,000)(0.0026)}{(3.0)(0.25)} = 236 \text{ lb}$$

To calculate the maximum deflection of the beam under a steady load, the creep modulus (Ea) is used rather than the flexural modulus. Because material properties are time dependent, a finite period is selected. In this example, maximum deflection after 100 hours is calculated.

The creep modulus at 100 hours can be estimated by dividing the steady load recommended maximum working stress from Table 35 by the assumed maximum strain (1.5%).

$$E_a = \frac{17,000 \text{ psi}}{0.015} = 1.13 \times 10^6 \text{ psi}$$

Substituting:

$$Y_{\max} = \frac{WL^3}{48E_a I} = \frac{(236)(3.0)^3}{(48)(1.13 \times 10^6)(0.0026)} = 0.045 \text{ in}$$

Maximum deflection at L/2 is predicted to be 1.2 mm.

Example 3 – Cyclic load

When materials are stressed cyclically, failures will occur at stress levels lower than the material's ultimate strength due to fatigue. To calculate the maximum cyclic load our beam can handle for a minimum of 10,000,000 cycles:

$$W_{\max} = \frac{4S_{\max}I}{Lc} = \frac{(4)(4550)(0.0026)}{(3.0)(0.25)} = 63 \text{ lb}$$



Stress Concentration

Part discontinuities, such as sharp corners and radii, introduce stress concentrations that may result in failure below the recommended maximum working stress. It is, therefore, critical that a part be designed so that the stress field is as evenly distributed as possible.

Circular perforations give rise to stress concentrations, but as Figure 50 demonstrates, Torlon® PAI is less sensitive than metal.

Maximum Working Stresses for Torlon® PAI Resins

Part design method of fabrication and end use conditions can restrict the allowable working stresses for a structural member. Prototype evaluation is the best method of determining the suitability of Torlon® PAI parts. The data summarized in Table 35 are useful early in the design process for use in the engineering equations for the proposed part.

Figure 50: Stress concentration factor for circular stress raiser (elastic stress, axial tension)

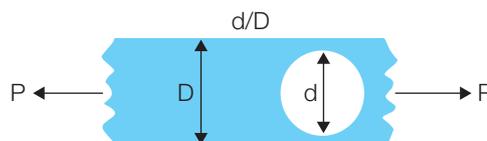
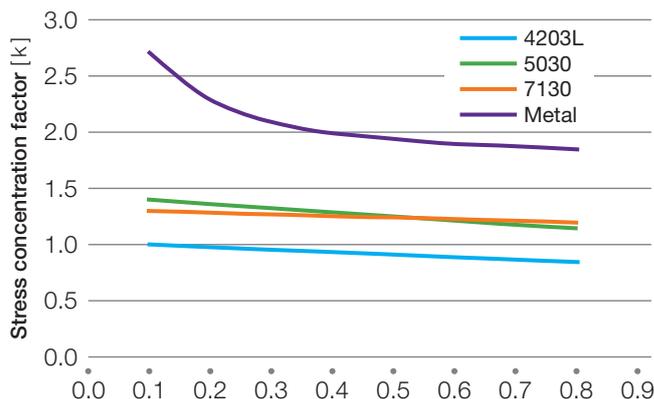


Table 35: Maximum working stresses for injection molded Torlon® PAI resins

Temperature	Units	Grade							
		4203L	4301	4275	4435	4630	4645	5030	7130
Short term load⁽¹⁾									
23°C (73°F)	MPa (psi)	117 (17,000)	96 (14,000)	89 (13,000)	66 (9,600)	49 (7,100)	74 (10,800)	122 (17,800)	121 (17,600)
135°C (275°F)	MPa (psi)	69 (10,000)	67 (9,800)	67 (9,800)	54 (7,800)	40 (5,800)	66 (9,500)	96 (13,900)	94 (13,700)
232°C (450°F)	MPa (psi)	39 (5,700)	44 (6,400)	34 (4,900)	31 (4,500)	32 (4,700)	58 (8,400)	67 (9,800)	55 (9,400)
Steady load (creep), <1.5% strain, 100 hrs.									
23°C (73°F)	MPa (psi)	48 (7,000)	69 (10,000)	65 (9,500)	-	-	-	117 (17,000)	117 (17,000)
93°C (200°F)	MPa (psi)	45 (6,500)	52 (7,500)	54 (7,900)	-	-	-	103 (15,000)	103 (15,000)
204°C (400°F)	MPa (psi)	34 (5,000)	41 (6,000)	41 (6,000)	-	-	-	69 (10,000)	69 (10,000)
Cyclic load, 10⁷ cycles									
23°C (73°F)	MPa (psi)	26 (3,850)	21 (3,000)	19 (2,800)	14 (2,000)	-	-	31 (4,550)	36 (5,250)
135°C (275°F)	MPa (psi)	17 (2,450)	14 (2,100)	14 (2,100)	11 (1,620)	-	-	24 (3,500)	29 (4,200)
232°C (450°F)	MPa (psi)	10 (1,400)	9 (1,350)	7 (1,050)	6 (950)	-	-	17 (2,450)	19 (2,800)



Designing with Torlon® PAI Resin

Fabrication Options

Torlon® PAI can be molded using any of three conventional molding techniques; injection molding, extrusion and compression molding. Each has advantages and limitations.



Injection Molding

Torlon® PAI parts can be injection molded to fine detail. Of the three methods, injection molding produces parts of the highest strength. When a large quantity of complex parts is required, injection molding can be the most economical technique due to short cycle times and excellent replication. Part thickness is limited by the flow length versus thickness relationship of the polymer. Thickness is limited to a maximum of 15.9 mm (0.625 inch).

Extrusion

Torlon® PAI polymers can be extruded into profiles and shapes such as rods, tubing, sheet, film and plates. Small parts with simple geometries can be economically produced by combining extrusion molding and automatic screw machining. Torlon® PAI rod and plate stock are available in a variety of sizes.

Compression Molding

Large parts over 15.9 mm (0.625 inch) thick must be compression-molded. Tooling costs are considerably lower compared with other molding techniques. Compression-molded parts will generally be lower in strength than comparable injection-molded or extruded parts, but have lower stresses and are therefore easier to machine. Compression molded rod, OD/ID tube combinations and compression molded plates are available in a variety of sizes and thickness. Contact your Solvay Specialty Polymers representative for information on approved sources.

Post-Curing Torlon® PAI Parts

Torlon® PAI parts must be post-cured. Optimal properties, especially chemical and wear resistance, are only achieved with thorough post-cure. Best results are obtained when Torlon® PAI parts are cured through a cycle of increasing temperature. Cure cycle parameters are a function of the size and geometry of a particular part.



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Guidelines for Designing Torlon® PAI Parts

Torlon® PAI can be precision molded to fine detail using a wide range of fabricating options. Not only can the designer select a material with outstanding performance, but one which gives him a great deal of design freedom.

The following sections provide guidelines for designing parts with Torlon® PAI.

Wall section

Whenever feasible, wall thickness should be minimized within the bounds prescribed by the end-use, to shorten cycle time and economize on material. When sections must be molded to thicknesses in excess of 12.7 mm (0.5 inch), parts may incorporate core and rib structures, or special Torlon® PAI grades may be used.

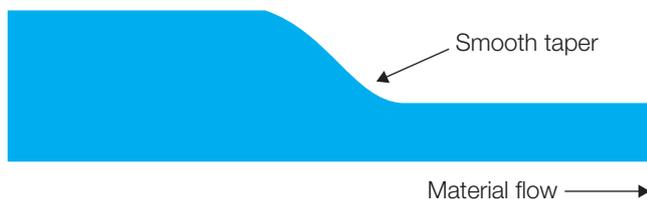
For small parts molded with Torlon® PAI resin, wall sections generally range from 0.8 to 13 mm (0.03 to 0.50 inch), but thicknesses up to 15.9 mm (0.625 inch) are possible with reinforced or bearing grades.

Torlon® PAI has a relatively high melt viscosity, which limits flow length for a given wall thickness. Use of hydraulic accumulators and precise process control reduce the impact of this limitation. Many factors, such as part geometry, flow direction, and severity of flow path changes make it difficult to characterize the relationship between flow length and wall thickness for sections less than 1.3 mm (0.050 inch) thick. We suggest you contact your Solvay Technical Representative to discuss the part under consideration.

Wall transition

Where it is necessary to vary wall thickness, gradual transition is recommended to eliminate distortion and reduce internal stresses. Figure 51 shows the desired method of transition, a smooth taper. It is better that the material flows from thick to thin sections to avoid molding problems such as sinks and voids.

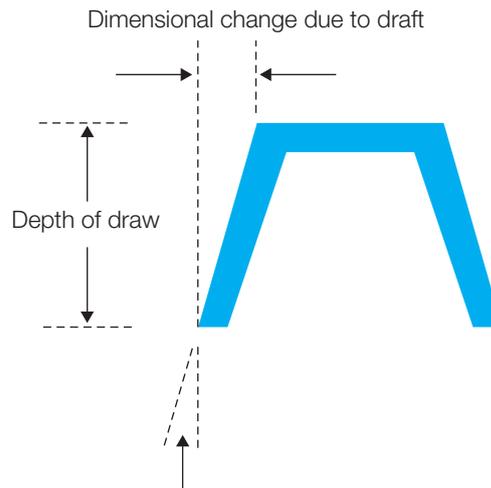
Figure 51: Gradual blending between different wall thicknesses



Draft angle

0.5° to 1° draft should be allowed to facilitate removal of the part from the mold. With Torlon® PAI resin, draft angles as low as one-eighth degree have been used, but such low angles require individual analysis. Draft angle is also dependent on the depth of draw; the greater the depth of draw, the greater the required draft angle (see Figure 52). Part complexity will also affect draft requirements, as will the texture of the finish. A textured finish generally requires 1° per side for every 0.025 mm (0.001 inch) of texture depth.

Figure 52: Considerations required for draft



Coresh

Coring is an effective way to reduce wall thickness in heavy sections. To minimize mold cost, core removal should be parallel to the movement of the platens.

Draft should be added to core design. Blind cores should be avoided, but if necessary, the general guidelines are: for cores less than 4.8 mm (0.1875 inch) diameter, the length should be no greater than twice the diameter; if greater than 4.8 mm (0.1875 inch), length should not exceed three times the diameter. For cored-through holes, length should not exceed six times the diameter for diameters over 4.8 mm (0.1875 inch), and four times the diameter for diameters less than 4.8 mm (0.1875 inch).



Ribs

Ribs can increase the stiffness of Torlon® PAI parts without increasing section thickness. The width of the rib at the base should be equal the thickness of the adjacent wall to avoid backfill. Ribs should be tapered for mold release.

Bosses

Bosses are commonly used to facilitate alignment during assembly, but may serve other functions. In general, the outer diameter of a boss should be equal to or greater than twice the inside diameter of the hole, and the wall thickness of the boss should be less than or equal to the adjacent wall thickness.

Undercuts

It is not possible to mold undercuts in Torlon® PAI parts unless side pulls are used. To minimize mold costs, undercuts should be avoided. If it is necessary, external undercuts can be accommodated by use of a side pull, but internal undercuts require collapsing or removable cores.

Molded-in inserts

Threads molded into Torlon® PAI parts have good pull-out strength, but if greater strength is needed, metal inserts can be molded-in. Torlon® PAI resins have low coefficients of thermal expansion, making them excellent materials for applications integrating plastic and metal. For ease of molding, inserts should be situated perpendicular to the parting line and should be supported so they are not displaced during injection of the molten plastic. Inserts should be preheated to the temperature of the mold.

Table 36 defines the ratio of the wall thickness of polymer around the insert to the outer diameter of the insert for common insert materials. Sufficient polymer surrounding the insert is necessary for strength.

Table 36: Wall thickness/insert Outer Diameter (OD) relationship

Insert Material	Ratio of Wall Thickness to Insert OD
Steel	1.2
Brass	1.1
Aluminum	1.0

Threads

Threads can be molded-in. Both internal and external threads can be molded using normal molding practices to Class 2 tolerance using Torlon® PAI resins. Class 3 can be molded using very high precision tooling. In general, it is more economical to machine threads for short runs. Table 39 on page 42 shows the screw holding strength of Torlon® PAI threads.

Holes

Holes can serve a variety of functions. Electrical connectors, for example, have numerous small holes in close proximity. Associated with each hole is a weld line which potentially is a weak point. The degree of weakness is related to flow distance, part geometry, and the thickness of the wall surrounding the hole. Because Torlon® PAI resins can be molded to close tolerances, and can be molded to thin cross sections without cracking, they are excellent materials for this type of part; however, each application must be considered on an individual basis due to the complexity of design variables.



Secondary Operations

Joining

Torlon® PAI parts can be joined mechanically or with adhesives.

Mechanical Joining Techniques

The dimensional stability and creep resistance of Torlon® PAI allows it to be readily joined with metal components even in rotating or sliding assemblies.

Snap-fit: Economical and simple

Snap-fit is an economical and simple method of joining Torlon® PAI parts. Although the strain limit must be considered for a snap-fit assembly that will be repeatedly assembled and disassembled, Torlon® PAI polymers are excellent for this type of use, due to the superior fatigue strength of polyamide-imide. The high modulus, elongation, and low creep of Torlon® PAI resins also make them well suited for snap-fit designs. Snap-in fingers in the locked position should be strain-free, or under a level of stress which can be tolerated by the material. Torlon® PAI resins can tolerate up to 10% strain for the unfilled grades, and 5% strain for filled grades. Graphite-fiber-reinforced grades are not suitable for snap-fit assembly.

Threaded Fasteners

Self-tapping screws

In general, Torlon® PAI is too tough for self-tapping screws. Tapped holes are recommended.

Molded-in inserts

Metal inserts can be molded into Torlon® PAI parts. Preheating the insert to the temperature of the mold is required for best results. While polyamide-imide has low shrink, it is still important to have sufficient material around the insert to distribute the stress induced by shrinkage.

Threaded mechanical inserts

Self-threading, self-locking inserts provide a high-strength, low-stress option for joining Torlon® PAI parts. These metal inserts have an exterior “locking” feature for anchorage in the Torlon® PAI part and allow for repeated assembly and disassembly through the threaded interior. HeliCoil® inserts from HeliCoil Products, division of Mite Corporation, and SpeedSerts® inserts from Tridair Fasteners, Rexnord, Incorporated, are examples of this type of insert.

Table 37 gives the tensile strength of HeliCoil® inserts in Torlon® 4203L and 5030. It is the axial force required to pull the insert at least 0.51 mm (0.020 inch) out of Torlon® PAI specimens.

Table 37: Strength of HeliCoil® inserts

Thread Size	Tensile Strength				
	#4-40	#6-32	#8-32	#10-32	¼"-20
Engagement					
mm	5.7	7.0	8.3	9.6	12.7
inch	0.224	0.276	0.328	0.380	0.500
4203L					
N	3,870	6,540	8,180	9,790	12,600
lbf	870	1,470	1,840	2,200	2,830
5030					
N	4,310	7,560	9,520	13,100	23,100
lbf	970	1,700	2,140	2,940	5,200

Molded-in threads

Both external and internal threads can be molded with Torlon® PAI polymer to a Class 2 tolerance. Mating parts with metal fasteners in Torlon® PAI threads works well because the thermal expansion of Torlon® PAI is close to that of metal, so there is relatively low thermal stress at the metal-to-plastic interface. Due to the increase in mold cost, it is generally advisable to machine threads for short runs.

Strength of bolts made of Torlon® PAI resin

Threaded fasteners molded from Torlon® PAI polymers are dependable because of the high strength, modulus, and load-bearing characteristics of Torlon® PAI polymers. Bolts were injection molded from Torlon® 4203L and 5030 then tested for tensile strength, elongation, and torque limit (Table 38). The bolts were 6.3 mm (0.25 inch) diameter, type 28TPI with class 2A threads. Tensile strength calculations were based on 0.235 cm² (0.0364 in²) cross sectioned area. Torque tests were conducted by tightening the bolts on a steel plate with steel washers and nuts. Maximum shear torque was determined using a torque wrench graduated in inch-pounds.

Table 38: Strength of Torlon® PAI bolts

Grade	Tensile Strength		Elongation	Shear Torque	
	[MPa]	[psi]		[Nm]	[inch·lb]
4203L	125	18,200	9.5	3.	
5030	127	18,400	6.6	3.	



Screw holding strength

Metal screws can securely join threaded Torlon® PAI parts. Holes for #4 – 40 screws were drilled and tapped in 4.8 mm (0.19 inch) thick Torlon® PAI plaques. Screw pull-out strength determined by ASTM D1761 appears in Table 39. Crosshead speed was 2.5 mm (0.1 inch) per minute. The span between the plaque and the screw holding fixture was 27 mm (1.08 inch).

Table 39: Screw holding strength of threads in Torlon® PAI

Grade	Pull-out Strength		Engagement Threads per Hole
	[kg]	[lb]	
4203L	240	540	7.5
4275	180	400	7.7
4301	200	460	7.8

Interference fits

Interference, or press, fits provide joints with good strength at minimum cost. Torlon® PAI engineering polymer is ideal for this joining technique due to its resistance to creep. Diametrical interference, actual service temperature, and load conditions should be evaluated to determine if stresses are within design limits.

Ultrasonic inserts

Metal inserts can be imbedded in uncured Torlon® PAI parts by ultrasonic insertion. Inserts are installed rapidly with strength comparable to that provided by molded-in techniques. A hole is molded slightly smaller than the insert. The metal insert is brought in contact with the Torlon® PAI part. Vibration in excess of 18 kHz is applied to the metal insert, creating frictional heat which melts the plastic. High strength is achieved if sufficient plastic flows around knurls, threads, etc.

Other mechanical joining techniques

Because post-cured Torlon® PAI parts are extremely tough, some joining techniques will not be suitable. Expansion inserts are generally not recommended; however, each application should be considered on an individual basis.

Bonding with Adhesives

Torlon® PAI parts can be joined with commercial adhesives, extending design options. It is a good practice to consult the adhesive supplier concerning the requirements of your application.

Adhesive choice

A variety of adhesives including amide-imide, epoxy, and cyanoacrylate can be used to bond Torlon® PAI parts. Cyanoacrylates have poor environmental resistance and are not recommended. Silicone, acrylic, and urethane adhesives are generally not recommended unless environment conditions preclude other options. The amide-imide adhesive is made by dissolving 35 parts of Torlon® 4000T PAI powder in 65 parts of N-methylpyrrolidone.

Warning! NMP is a flammable organic solvent and the appropriate handling procedures recommended by EPA, NIOSH, and OSHA should be followed. Adequate ventilation is necessary when using solvents.

Bonding various Torlon® PAI grades

Torlon® PAI resin grades 4203L, 5030, and 7130 are relatively easy to bond. Bearing grades 4301, 4275, and 4435 have inherent lubricity, and are more difficult to bond. Table 40 compares the shear strengths of these grades bonded with epoxy, cyanoacrylate, and amide-imide adhesives.

Post-cured Torlon® PAI bars, 64 × 13 × 3 mm (2.5 × 0.5 × 0.12 inch) were lightly abraded, wiped with acetone, then bonded with a 13 mm (0.5 inch) overlap. The clamped parts were cured per the adhesive manufacturer's recommendations. After 7 days at room temperature, bonds were pulled apart with a tensile testing machine at a crosshead speed of 1.3 mm per minute (0.05 inch per minute). If failure occurred outside the bond area, the process was repeated with progressively smaller bond areas, to a minimum overlap of 3.2 mm (0.125 inch).

Surface preparation

Bonding surfaces should be free of contaminants, such as oil, hydraulic fluid, and dust. Torlon® PAI parts should be dried for at least 24 hours at 149 °C (300 °F) in a desiccant oven (thicker parts, over 6.3 mm (0.25 inch), require longer drying time) to dispel casual moisture prior to bonding. Torlon® PAI surfaces should be mechanically abraded and solvent-wiped, or treated with a plasma arc to enhance adhesion.



Design Guide



Adhesive application

For adhesives other than amide-imide, follow the manufacturer's directions. For amide-imide adhesive: coat each of the mating surfaces with a thin, uniform film of the adhesive. Adhesive-coated surfaces should be clamped under minimal pressure, approximately 0.25 psi (1.7 KPa). The excess adhesive can be cleaned with N-methylpyrrolidone (NMP).

Warning! NMP is a flammable organic solvent and the appropriate handling procedures recommended by EPA, NIOSH, and OSHA should be followed. Adequate ventilation is necessary when using solvents.

Curing procedure

Amide-imide adhesive should be cured in a vented, air-circulating oven. The recommended cycle is 24 hours at 23 °C (73 °F), 24 hours at 149 °C (300 °F), 2 hours at 204 °C (400 °F). The parts should remain clamped until cooled to below 66 °C (150 °F).

Bond strength of various adhesives

Commercial adhesives were used to bond Torlon® PAI parts. The bonds were evaluated for shear strength, which appears in Table 40.

Method of cure, handling, and working life of the adhesive are rated in terms of "ease of use". Useful temperature ranges appear in the manufacturers' literature and will vary with factors such as load and chemical environment.

Bonding Torlon® PAI parts to metal

Torlon® PAI and metal parts can be joined with adhesives. With proper surface preparation and adhesive handling, the resulting bonds will have high strength. In addition, there will be minimal stress at the interface with temperature change. This is because Torlon® PAI resins, unlike many other high temperature plastics, have expansion coefficients similar to those of metals.

As mentioned in the preceding section, bond strength depends on adhesive selection, and Torlon® PAI grade, as well as proper technique in preparing and curing the bond. Table 41 reports shear strength data for Torlon® PAI to aluminum and Torlon® PAI to steel bonds. Mechanical abrasion alone may not be adequate for preparing steel surfaces – chemical treatment of the steel is recommended when service temperature requires the use of amide-imide adhesive.



Table 40: Shear strength of Torlon® PAI-to-Torlon® PAI Bonds

Grade	Unit	Epoxy ⁽¹⁾	Cyanoacrylate ⁽²⁾	Amide-imide
4203L	MPa (psi)	41.4 (6,000+)	19.2 (2,780)	34.5 (5,000+)
4301	MPa (psi)	15.5 (2,250)	12.0 (1,740)	19.9 (2,890)
4275	MPa (psi)	24.1 (3,500)	11.6 (1,680)	23.4 (3,400)
5030	MPa (psi)	33.0 (4,780)	21.2 (3,070)	35.4 (5,140)
7130	MPa (psi)	44.1 (6,400+)	27.4 (3,980)	32.8 (4,750)
Ease of use 1= easiest		2	1	3
Useful temperature range	°C (°F)	-55 to 71 (-67 to 160)	-29 to 99 (-20 to 210)	-196 to 260 (-321 to 500)

⁽¹⁾ Hysol® EA 9330. Hysol is a trademark of Dexter Corporation⁽²⁾ CA 5000. Lord Corporation**Table 41:** Shear strength of Torlon® PAI-to-Metal Bonds⁽¹⁾

Grade	Unit	Epoxy ⁽²⁾	Cyanoacrylate ⁽³⁾	Amide-imide
Shear strength–Aluminum 2024 to Torlon® PAI bonds				
4203L	MPa (psi)	27.6 (4,000)	9.3 (1,350)	34.8+ (5,050+)
4301	MPa (psi)	17.2 (2,500)	10.0 (1,450)	34.1+ (4,950+)
4275	MPa (psi)	16.9 (2,450)	5.2 (750)	30.0+ (4,350+)
5030	MPa (psi)	26.9 (3,900)	22.4 (3,250)	41.7+ (6,050+)
7130	MPa (psi)	27.6 (4,000)	25.9 (3,750)	44.1+ (6,400+)
Shear strength–Cold rolled steel to Torlon® PAI bonds				
4203L	MPa (psi)	21.0 (3,050)	15.2 (2,200)	10.0 (1,450)
4301	MPa (psi)	25.5 (3,700)	14.1 (2,050)	12.7 (1,850)
4275	MPa (psi)	21.7 (3,150)	16.9 (2,450)	13.1 (1,900)
5030	MPa (psi)	32.1 (4,650)	14.5 (2,100)	16.5 (2,400)
7130	MPa (psi)	31.4 (4,550)	16.9 (2,450)	7.6 (1,100)
Ease of use 1= easiest		2	1	3
Useful temperature range	°C (°F)	-55 to 71 (-67 to 160)	-29 to 99 (-20 to 210)	-196 to 260 (321 to 500)

⁽¹⁾ This test used Torlon® PAI bars 64 × 13 × 3 mm (2.5 × 0.5 × 0.125 inch); steel strips of similar size were cut from cold rolled steel, dull finished panel; and aluminum strips were cut from 2024 alloy panels.⁽²⁾ Hysol EA 9330. Hysol is a trademark of Dexter Corporation⁽³⁾ CA 5000. Lord Corporation

Design Guide

塑料专家 www.ponci.com.cn/wxb/ +13538586433 +18816996168



Guidelines for Machining Parts Made from Torlon® PAI Resin

Molded shapes and extruded bars manufactured from Torlon® PAI can be machined using the same techniques normally used for machining mild steel or acrylics. Machining parameters for several typical operations are presented in Table 42.

Parts made from Torlon® PAI resin are dimensionally stable, and do not deflect or yield as the cutting tool makes its pass. All Torlon® PAI grades are very abrasive to standard tools, and high-speed tools should not be used.

Carbide-tipped tools may be used, but diamond-tipped or insert cutting tools are strongly recommended. These tools will outlast carbide-tipped tools and provide a strong economic incentive for production operations, despite a relatively high initial cost. Thin sections or sharp corners must be worked with care to prevent breakage and chipping. Damage to fragile parts can be minimized by using shallow cuts during finishing operations. The use of mist coolants to cool the tool tip and to help remove chips or shavings from the work surface is recommended. Air jets or vacuum can be used to keep the work surface clean.

Parts machined from injection-molded blanks may have built-in stresses. To minimize distortion, parts should be machined symmetrically, to relieve opposing stresses.

Machined parts should be recured

Parts designed for friction and wear-intensive service, or which will be subjected to harsh chemical environments, should be recured after machining to insure optimum performance. If such a part has been machined to greater than 1.6 mm (0.0625 inch) depth, recuring is strongly recommended.

Table 42: Guidelines for machining parts made from Torlon® PAI resin

Turning	Value	Unit
Cutting speed	90 – 240	m/min
Feed	0.1 – 0.6	mm/rev
Relief angle	5 – 15	degrees
Rake angle	7 – 15	degrees
Cutting depth	0.6	mm
Circular Sawing		
Cutting	1,800 – 2,400	m/min
Feed	fast & steady	in/rev
Relief angle	15	degrees
Set	slight	
Rake angle	15	degrees
Milling		
Cutting speed	150 – 240	m/min
Feed	0.2 – 0.9	mm/rev
Relief angle,	5 – 15	degrees
Rake angle	7 – 15	degrees
Cutting depth	0.9	mm
Drilling		
Cutting speed	90 – 240	m/min
Feed	0.1 – 0.4	mm/rev
Relief angle	0	degrees
Point angle	118	degrees
Reaming		
Slow speed	150	m/min



Index

A		
Absorption Rate	24	
Adhesive Application	43	
Adhesive Choice	42	
Aircraft Hydraulic Fluid (Skydrol® 500B)	23	
Aircraft Turbine Oil, With and Without Stress	23	
An Introduction to Torlon® PAI Wear-Resistant Grades	28	
ASTM D5204 Standard Classification System for Polyamide-imide (PAI) Molding and Extrusion Materials	34	
Automotive Lubricating Fluids	23	
B		
Bearing Design	33	
Bearing Design Concepts	28	
Bearings	28	
Bonding Torlon® PAI parts to metal	43	
Bonding Various Torlon® PAI Grades	42	
Bonding with Adhesives	42	
Bond Strength of Various Adhesives	43	
Bosses	40	
C		
Calculating the Pressure and Velocity	28	
Changes in Mechanical and Electrical Properties	25	
Chemical Resistance	21	
Chemical Resistance Under Stress	24	
Coefficients of Linear Thermal Expansion (CLTE)	15	
Compression Molding	38	
Compressive Properties	11	
Constraints on Sudden High Temperature Exposure	25	
Cores	39	
Curing Procedure	43	
D		
Designing with Torlon® PAI Resin	38	
Dimensional Changes	24	
Draft Angle	39	
E		
Effect of Mating Surface on Wear Rate	31	
Effects of Prolonged Thermal Exposure	14	
Effects of Water	24	
Electrical Properties	27	
Equilibrium Absorption at Constant Humidity	24	
Example 1 - Short-term loading	36	
Example 2 - Steady load	36	
Example 3 - Cyclic load	36	
Effect of Stress and Deflection on Adhesive Application	36	
Effect of Stress and Deflection on Adhesive Application	38	
F		
FAA Flammability	21	
Fabrication Options	38	
Fatigue Strength	12	
Federal Aviation Administration	34	
Flammability	19	
Fracture Toughness	13	
G		
Geometry and Load Considerations	36	
Guidelines for Designing Torlon Parts	39	
Guidelines for Machining Parts Made from Torlon® PAI Resin	45	
H		
High Performance Torlon® PAI Polymers	6	
Holes	40	
Horizontal Burning Test	20	
I		
Ignition Properties	19	
Impact Resistance	13	
Industry and Agency Approvals	34	
Injection Molding	38	
Interference Fits	42	
Introduction	5	
J		
Joining	41	
L		
Lubricated Wear Resistance	31	
M		
Machined Parts Should be Recured	45	
Material Efficiency—Specific Strength and Modulus	35	
Maximum Working Stresses for Torlon® PAI Resins	37	
Measuring wear resistance	29	
Mechanical Joining Techniques	41	
Military Specification MIL-P-46179A	34	
Molded-In Inserts	40, 41	
Molded-In Threads	41	
N		
National Aeronautics and Space Administration	34	
NBS Smoke Density	19	
O		
Other Mechanical Joining Techniques		
Oxygen Index		



P			
Performance in Various Environments	21	Thermal Conductivity	15
Performance Properties	9	Thermal Stability	13
Physical Properties	6	Thermogravimetric Analysis.	14
Post-Curing Torlon Parts	38	Threaded Fasteners	41
PV Limit Concept	29	Threaded Mechanical Inserts	41
		Threads.	40
R		Torlon® Polyamide-Imide (PAI)	5
Resistance To Automotive and Aviation Fluids	23	Torlon® PAI Polymers for Insulating	27
Resistance To Cyclic Stress	12	Torlon® PAI Wear-Resistant Grades	30
Resistance to Gamma Radiation	26	Toxic Gas Emission Test	19
Restoration of Dimensions and Properties.	24		
Retention of Properties After Thermal Aging	14	U	
Ribs.	40	UL 57 Electric Lighting Fixtures	21
		UL 94 Flammability Standard	19
S		UL Relative Thermal Index.	14
Screw Holding Strength	42	Ultra Low Temperature	10
Secondary Operations	41	Ultrasonic Inserts.	42
Self-Tapping Screws	41	Undercuts	40
Service in Wear-Resistant Applications	28	Underwriters Laboratories.	34
Snap-Fit: Economical and Simple	41		
Society of Automotive Engineers-Aerospace Material Specifications	34	V	
Specific Heat.	15	Vertical Burn Test	20
Strength of Bolts made of Torlon® PAI Resin	41		
Stress Concentration.	37	W	
Stress-Strain Relationship	11	Wall Section	39
Structural Design.	35	Wall Transition	39
Surface Preparation	42	Wear rate relationship	28
		Wear Resistance and Post-Cure	32
T		Weather-Ometer® Testing	26
Tensile and Flexural Strength at Temperature Extremes	9		
Tensile Properties Per ASTM Test Method D638	10		





Specialty Polymers

Worldwide Headquarters

SpecialtyPolymers.EMEA@solvay.com

Viale Lombardia, 20
20021 Bollate (MI), Italy

Americas Headquarters

SpecialtyPolymers.Americas@solvay.com

4500 McGinnis Ferry Road
Alpharetta, GA 30005, USA

Asia Headquarters

SpecialtyPolymers.Asia@solvay.com

No.3966 Jindu Road
Shanghai, China 201108

www.solvay.com

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